Longitudinal kinematic and kinetic adaptations to obstacle crossing in recent lower limb amputees

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Background

Transtibial amputees must perform numerous activities of daily living (ADL) of varying difficulty, including obstacle crossing. Obstacle crossing is an important ADL and is necessary to avoid a potential trip or fall and any subsequent falls-related injury. Therefore, the successful crossing of obstacles influences an individual's ability to maintain independence and subsequent quality of life.

Previous studies have shown that lower limb amputees are able to negotiate obstacles successfully, albeit with an inherent degree of altered mechanical functioning ^[1-6]. However, when compared to able-bodied individuals, transtibial amputees negotiated obstacles more slowly ^[4] and made contact with obstacles more often under increasing time pressure ^[3, 5]. Encouragingly, these deficits have been shown to diminish in individuals with greater time since amputation in cross-sectional studies ^[3]. Therefore, there is a need to monitor adaptations longitudinally.

A lead limb preference (LLP) (Figure 1) reflects an amputee's preferred obstacle crossing strategy and the lack of a clear LLP may be indicative of increased adaptability when performing this motor task. Equivocal findings with regards to LLP, and the potential mechanisms responsible for LLP selection, highlight the lack of a clear consensus within the literature as to the best strategy of crossing an obstacle in lower limb amputees ^[1, 4]. The propulsive mechanism achieved via ankle plantarflexion in pre-swing, prior to the limb crossing the obstacle, has been cited as a reason for choosing an intact LLP ^[2]. Conversely, reduced knee joint range of motion (ROM) owing to the physical constraints of the posterior shell of the prosthesis and socket fit have been proposed to reduce the suitability of an affected trail limb ^[1, 1].

^{2]}. When leading with the affected limb, compensatory mechanisms such as increased intact limb ankle plantarflexion and affected limb knee and hip flexion have been reported to facilitate obstacle clearance ^[1]. Moreover, reduced affected limb knee ROM upon landing purportedly indicates an inability to effectively control musculature about the knee in preparation for the subsequent stance phase ^[2, 3].

Results from previous studies have been largely obtained from amputees with a number of years of prosthetic experience ^[1-5] with few investigations assessing the longitudinal changes that occur in more recent amputees ^[6]. However, given that recent amputees are likely to be more receptive to adaptations to their movements, these investigations have important implications with regards to improving locomotor function, avoiding trips and falls, falls-related injuries and subsequent loss of mobility and independence in this population. The aim of the current study therefore was to investigate the longitudinal adaptations in recent transtibial amputees when crossing an obstacle positioned along a level walkway, during the six-month period following discharge from rehabilitation. It was predicted that walking velocity, an indicator of overall performance, would increase over time following discharge ^[7]. It was also predicted that improvements in overall performance would be due to the increased joint mobility and power bursts associated with the intact limb. Finally, it was predicted that LLP would change over time as participants adapted their movement strategies when crossing an obstacle.

Methods

Participants

Seven unilateral transtibial amputees gave informed consent to participate in the current study having completed a course of rehabilitation within a National Health Service (NHS) physiotherapy department (Table 1). Participants' rehabilitation was conducted by the same

clinicians in the same department and followed similar pathways including the initial use of early walking aids, followed by the practice of ADLs with an initial prescribed prosthetic limb. Participants were excluded if they had any current musculoskeletal injuries, cognitive deficits or experienced pain or discomfort whilst using their prostheses. Participants were included if they could complete a number of functional tasks without the use of a walking aid, including walking a distance of five metres and stepping over an obstacle. The study was approved by the NHS local research ethics committee (08/H1304/10).

Insert Table 1 here

Experimental Set-up

A polystyrene obstacle of 0.1m (height) and 1.0m (width) with supporting legs was positioned between two force platforms along a 10m walkway. Obstacle dimensions were wide enough to prevent negotiation of the obstacle by walking around it and high enough to represent items encountered on the floor during everyday living and corresponded to those previously reported ^[1, 4, 6]. A ten-camera motion capture system (Qualisys, Sweden) and two force platforms (Model 9281B, Kistler, Switzerland) sampled kinematic (100Hz) and ground reaction force (GRF) (1000Hz) data synchronously via Qualisys Track Manager software (Qualisys, Sweden). *Experimental Design and Protocol*

The current study utilised a repeated measures design with participants attending standardised data collection sessions at one, three and six months following discharge from rehabilitation. Participants wore their own comfortable, flat footwear and were able to fit and re-adjust their own prostheses prior to data collection. In accordance with the six degrees-of-freedom marker set ^[8-10], 14mm reflective markers were attached bilaterally to the calcaneus, 1st, 2nd and 5th metatarsals, medial and lateral aspects of the malleoli and femoral epicondyles, greater trochanter, iliac crest and anterior and posterior superior iliac spines. Four-marker rigid clusters

were attached to the thigh and shank segments. This marker set allowed for six degrees of freedom segmental kinematics to be recorded ^[8]. Marker placement on the affected limb was estimated from intact limb anatomical landmarks ^[7, 11]. A static calibration was performed by collecting kinematic data of each participant standing in the anatomical neutral position. Following completion of several practice trials, participants self-selected a starting position which was typically around 4m from the obstacle, before walking along the walkway and stepping over the obstacle at a self-selected velocity. A minimum of five trials were recorded. *Data Analysis*

A large number of gait variables were computed from this analysis and key variables are presented in the current study. Raw kinematic and GRF data were interpolated using a cubic-spline algorithm and filtered using a fourth-order low pass Butterworth filter in Visual 3D (C-Motion, Inc, Germantown, USA) with cut-off frequencies of 6Hz and 30Hz, respectively. Anatomical frames were defined using medial and lateral landmarks from which segment co-ordinate systems were defined following the right hand rule ^[8]. As participants crossed the obstacle, the transition steps were analysed (Figure 1). The lead limb was defined as the first limb to cross the obstacle, with the contralateral limb designated as the trail limb. Lead limb selection was not controlled for and was noted during each trial in order to assess lead limb preference (Figure 1). Walking velocity (m.s⁻¹) and stance duration (% gait cycle) were calculated along with joint angles (°) from the ankle, knee and hip. Peak vertical GRF was normalised to body weight (BW) with corresponding braking (Fz1) and propulsive (Fz2) peaks labelled. Normalised joint power (W/kg) data were calculated for the ankle, knee and hip with peak power burst values being presented ^[12]. Kinetic data were measured following obstacle crossing for the lead limb and prior to obstacle crossing for the trail limb (Figure 1). The gait

cycle was normalised from toe-off to the subsequent toe-off for the lead limb and from foot contact to subsequent foot contact for the trail limb (Figure 1).

Insert Figure 1 here

Statistical Analysis

Group mean data were analysed using a linear mixed model, Limb (Affected, Intact) * Time (One, Three and Six Months) with repeated measures on the last factor. This design allowed for the analysis of changes in multiple gait variables ^[13]. Each feature of the design (Time and Limb) was modelled as a fixed effect with the appropriate model being selected according to the lowest value for Hurvich and Tsai's Criterion (AICC). Underlying assumptions were checked using conventional graphical methods and were deemed plausible unless stated otherwise. In the instance of a significant result, post-hoc comparisons were conducted using a Sidak adjustment in SPSS v.17.0 (SPSS Inc., Chicago, USA). The alpha level of statistical significance was set at p≤0.05.

Results

No participants made contact with the obstacle during any visit to the laboratory. The majority of participants favoured an intact LLP, although this preference reduced by 10.6% from 68.8% to 58.2% between one and six months post-discharge (Table 2). As predicted, participants' walking velocity when crossing the obstacle, increased by 0.17m.s⁻¹ between one and six months post-discharge, regardless of LLP (Table 2). Intact limb stance duration was significantly greater whether it acted as the lead (p<0.01) or trail limb (p<0.01), with differences of 6% (lead limb) and 8% (trail limb) at six months post-discharge from rehabilitation. *Lead Limb Comparisons*

A significant interaction effect was reported for peak ankle dorsiflexon during swing (p=0.05) due to the increased ROM associated with the intact ankle joint when compared to the

prosthetic ankle joint. With an intact LLP, peak knee flexion during swing (p=0.03) and peak knee flexion during loading after touch-down (p=0.04) were significantly greater when compared to an affected LLP (Table 2). No statistically significant effects were observed for variables pertaining to the hip in the lead limb.

Having crossed the obstacle, load rate (p=0.05) and second peak vertical GRF (Fz2) (p=0.03) were significantly higher when leading with the intact vs. affected limb (Figure 2, Table 3). Statistically significant time main effects were reported for Fz2 (p=0.05) and decay rate (p=0.05) (Figure 2, Table 3). There were no statistically significant effects associated with lead limb first peak vertical GRF (Fz1).

Peak ankle power generation (A2) (p=0.01), knee power absorption (K3) (p=0.05) and hip power generation (H3) (p=0.05) during pre-swing following obstacle crossing as well as peak knee power absorption during swing (K4) (p=0.01) prior to obstacle crossing were all higher when leading with the intact limb compared to leading with the affected limb (Figure 2, Table 3). There were no further statistically significant effects associated with lead limb peak joint power bursts.

Insert Table 2 Here

Insert Figure 2 Here **Insert Table 3 Here** Trail Limb Comparisons During swing, as the trail limb crossed the obstacle, peak ankle dorsiflexion was greater with the intact vs. affected limb (p<0.01). No other statistically significant effects were noted for trail limb joint kinematics or variables associated with GRF.

A significant interaction effect (p=0.02) was found for peak ankle power absorption during stance (A1) which increased steadily between one and six months when trailing with the affected limb but was reduced in magnitude when compared to the intact limb (Figure 2, Table 3). Similarly, increases observed in peak ankle power generation (A2) between one and six months were statistically significant (p=0.05), although the magnitude of power burst A2 was consistently greater throughout with an intact vs. affected trail limb strategy (p=0.02) (Figure 2, Table 3). Peak knee power absorption (K1) (p=0.04) and generation (K2) (p=0.02) during early stance were greater when trailing with the intact limb vs. affected limb (Figure 2, Table 3). In addition, the increase and subsequent decrease in K1 between one and six months resulted in a significant time main effect (p=0.05) (Table 3). Changes in peak knee power generation during pre-swing (K3) were statistically significant between one and three months (p=0.05) (Table 3). However these changes were not uniform, with a decrease associated with an intact limb trail strategy and an increase associated with an affected limb trail strategy. There was a large, statistically significant inter-limb difference in peak knee power absorption during terminal swing (K4), due to the increased magnitude of power absorption when trailing with the intact limb (p=0.01) (Figure 2, Table 3). There were no statistically significant effects associated with trail limb peak hip joint power bursts.

Discussion

The aim of the current study was to investigate the biomechanical adaptations in recent transtibial amputees when crossing an obstacle, during the six-month period following discharge

from rehabilitation. As predicted and independent of LLP, walking velocity increased by 0.17m.s⁻¹ between one and six months post-discharge. Whilst not statistically significant, this 24% increase was considered a clinically meaningful improvement in performance within the sixmonth timeframe as walking velocity reflects an individual's overall locomotor ability ^[7]. In addition, no trips or falls occurred during the performance of the task which was important given the safety concerns of performing such ADLs for this group. These results corroborated findings from previous studies and the assertion that transtibial amputees are able to negotiate obstacles successfully ^[1-6].

Results from the current study suggest that the increased capacity of the intact limb to perform the role of the lead limb may explain the LLP observed. As predicted, knee flexion and power absorption during swing were greater when leading with the intact limb compared to the affected limb. This increased intact limb knee ROM and control during the approach and initial stage of obstacle crossing, may reflect participants' increased confidence of avoiding contact of the intact limb with the obstacle. Unintentional lead limb contact with the obstacle would necessitate corrective movements in order to avoid tripping or falling which may be more effective with the intact limb. Concurrently, the affected limb, which is supporting body weight during the critical single limb support phase, may also be required to provide corrective movements in the case of obstacle contact. Previous research has suggested that postural adjustment originating from the affected limb during stance phase may not be as complex as kinematic adjustments during swing ^[3].

As predicted, a number of variables indicative of stance phase function such as stance duration, knee joint ROM, load rate and peak power generation (A2) and absorption (K3), were increased

upon landing after the obstacle when leading with the intact limb. Previous literature has suggested a number of mechanisms responsible for the selection of an intact LLP such as the enhanced ability to push off with the intact limb at the end of the preceding stance phase ^[2] and the reduced affected limb control during swing, resulting in instability in preparation for the subsequent stance phase ^[2, 3]. This highlights the importance of the role of the lead limb having crossed the obstacle during a potentially vulnerable stage of obstacle crossing when the contralateral (affected) limb is in swing. This is an important consideration for those involved in the rehabilitation of lower limb amputee obstacle crossing as lead limb stance phase function will help to prevent tripping or falling. Results from the current study suggest that in the early stages following rehabilitation, the intact limb was not more accomplished or preferred in performing this role. However, circumstances may require the use of an affected lead limb strategy. Therefore, additional gains in affected lead limb function is important for further overall improvement in function and adaptability of amputee obstacle crossing performance.

Previous literature has reported equivocal findings with regards to LLP ^[1, 4], although individual and study sample differences may partially account for these discrepancies. In the current study, participants generally self-selected an intact LLP although, as predicted, there was an increase in the use of an affected limb LLP over time providing an insight into the obstacle crossing strategies of transtibial amputees. Significant time main effects were observed in ankle and knee kinetic variables during the stance phase of the trail limb, including increased power generation and absorption at the ankle. This suggests that participants improved their ability to utilise the passive function of the prosthetic ankle and active function of the biological ankle during stance which may help to explain the changes in LLP over time.

The influence of rehabilitation practices must also be considered. Initially, amputees are often advised to cross obstacles leading with their 'strongest' limb which, during and shortly following rehabilitation, is likely to encourage an intact LLP. However, with time following rehabilitation, improved prosthetic confidence and practice of locomotor tasks, the LLP is liable to change ^[3, 7] as observed in the current study, which is possibly reflective of increased and more adaptable obstacle crossing ability. These results also suggest that immediately following discharge from rehabilitation and for at least six months, amputees' locomotor function is malleable and particularly sensitive to intervention, whether through formal clinical treatment or home-based activity. These novel findings advocate the importance of continuing strength and flexibility training following discharge from rehabilitation, with recommendations for follow-up visits at regular intervals to monitor progress.

Previous studies have suggested that an affected LLP allows amputees to control the limb during swing via visual feedback ^[1, 4] and provides increased time to prepare the limb for stance ^[4]. However, the intact LLP observed and inter-limb differences outlined in the current study are in contrast to these suggestions. Despite these equivocal findings, one implication of these results is that the flexibility to adopt an affected LLP may be necessary when encountering an unexpected obstacle. Practicing obstacle crossing during rehabilitation in addition to improving joint ROM, muscle strength and enhanced prosthetic design may increase amputees' ability to perform these tasks safely and confidently ^[3-6]. The current study findings advocate these suggestions, which have implications for those involved in the care and rehabilitation of a timeframe during which the system is more responsive to further change could be very important for improving an amputee's confidence and performance of more complex ADLs. This

may in turn help to reduce the intact LLP bias established during rehabilitation and thereby improve the ability to cross unexpected obstacles safely and reduce the potential for subsequent falls and falls-related injury. Future investigations should focus on examining the effects of interventions, such as advanced rehabilitation or home-based therapy, aimed at improving affected limb strength, on amputees' performance of complex ADLs following discharge from rehabilitation when amputees' motor patterns are more receptive to change.

The results from the current study have highlighted a number of possible mechanisms that lead to the establishment of an intact LLP and have outlined the key role played by the intact limb in the six-month period following rehabilitation. However, limitations of the current study must be acknowledged. Several variables were adapted favourably and often improved in the six-month period following discharge, with some of these effects being statistically significant. This was encouraging in that performance of obstacle crossing improved without the specific clinical interventions or guidance advocated in the current study. However, the magnitude of time main effects was not as great as the limb main effects. It is likely that the relatively small sample size and subsequently reduced statistical power, may have resulted in the more subtle changes over time not reaching statistical significance. In addition, it could be suggested that the variation in the cause of amputation may have introduced some additional variance in the measures reported. However, more recent amputees are likely to still be adapting to the novelty of the mechanical constraints of the lower limb in the six months following discharge from rehabilitation, Participants in the current study had an amputation related to either traumatic or vascular reasons, and irrespective of cause, lower limb amputees are likely to be responsive to further treatment in the six months following discharge from rehabilitation. Future research should attempt to investigate the long-term adaptations in function of lower limb amputees

secondary to a range of causes, as this information would be valuable to those involved in the care and rehabilitation of lower limb amputees by highlighting cause-specific patient requirements. Finally, participant were discharged from rehabilitation once they had achieved the individual goals established with their care team and had a comfortable level of function. This process varies in length of time and number of treatments depending on the individual. However, as this is more reflective of the population's experience, the results are more generalisable to the wider amputee population.

Conclusion

Despite the greater reliance on intact limb function, changes in walking velocity, LLP and lower limb kinetics suggested that obstacle crossing in the current participant group improved over six months with inter-limb biomechanical mechanisms being highlighted. In the six-month period following discharge from rehabilitation, amputees may be positively susceptible to further improvements in performance and prosthetic confidence. The findings from this study suggest that the introduction of obstacle crossing during rehabilitation, improvements to prosthetic design and therapeutic interventions addressing the joint ROM and limb strengthening issues may help to improve amputees' capacity when performing obstacle crossing.

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Declaration of Conflicting Interests

The Authors declare there no conflict of interest.

References

1. Hill SW, Patla AE, Ishac MG, Adkin AL, Supan TJ and Barth DG. Kinematic patterns of participants with a below-knee prosthesis stepping over obstacles of various heights during locomotion. Gait Posture 1997; 6: 186-192

2. Hill SW, Patla AE, Ishac MG, Adkin AL, Supan TJ and Barth DG. Altered kinetic strategy for the control of swing limb elevation over obstacles in unilateral below-knee amputee gait. J Biomech 1999; 32: 545-549

3. Hofstad CJ, van der Linde H, Nienhuis B, Weerdesteyn V, Duysens J and Geurts AC. High failure rates when avoiding obstacles during treadmill walking in patients with a transtibial amputation. Arch Phys Med Rehabil 2006; 87: 1115-1122

4. Vrieling A, Van Keeken H, Schoppen T, Otten E, Halbertsma J, Hof A and Postema K. Obstacle crossing in lower limb amputees. Gait Posture 2007; 26: 587-594

5. Hofstad CJ, Weerdesteyn V, van der Linde H, Nienhuis B, Geurts AC and Duysens J. Evidence for bilaterally delayed and decreased obstacle avoidance responses while walking with a lower limb prosthesis. Clin Neurophysiol 2009; 120: 1009-1015

Vrieling AH, van Keeken HG, Schoppen T, Hof AL, Otten B, Halbertsma JPK and Postema K.
Gait adjustments in obstacle crossing, gait initiation and gait termination after a recent lower
limb amputation. Clin Rehabil 2009; 23: 659

7. Barnett C, Vanicek N, Polman R, Hancock A, Brown B, Smith L and Chetter I. Kinematic gait adaptations in unilateral transtibial amputees during rehabilitation. Prosthet Orthot Int 2009; 33: 135-147

 Cappozzo A, Catani F, Della Croce U and Leardini A. Position and orientation in space of bones during movement: anatomical frame definition and determination. Clin Biomech 1995; 10: 171-178

9. Collins TD, Ghoussayni SN, Ewins DJ and Kent JA. A six degrees-of-freedom marker set for gait analysis: Repeatability and comparison with a modified Helen Hayes set. Gait Posture 2009; 30: 173-180

10. Buczek FL, Rainbow MJ, Cooney KM, Walker MR and Sanders JO. Implications of using hierarchical and six degree-of-freedom models for normal gait analyses. Gait Posture 2010; 31: 57-63

11. Powers CM, Rao S and Perry J. Knee kinetics in trans-tibial amputee gait. Gait Posture 1998; 8: 1-7

12. Eng JJ and Winter DA. Kinetic analysis of the lower limbs during walking: what information can be gained from a three-dimensional model? J Biomech 1995; 28: 753-758

Brown H and Prescott R. Applied mixed models in medicine. 2nd ed. Chichester: Wiley,
2006, p. 215-249.





Lead Limb



■ Affected Limb Intact Limb

-4

-4

Months Post-Discharge

K4†

Months Post-Discharge

Gender (M/F)	Age (years)	Height (m)	Mass (kg)	Amputated Limb (R/L)	Cause of Amputation	Time Since Amputation (days)	Functional Prosthetic Components			
Μ	44	1.77	76.5	R	Non-Vascular	129	Renegade Freedom Foot*			
Μ	63 44	1.74	83.7 81.0	L R	Non-Vascular Non-Vascular		/ascular 123 Tres Foot with torque absorber S		Socket interface devices and pylons	
Μ		1.82					Renegade Freedom Foot*	were consistent over time. All participants used a patella tendon		
М	75 1.93		101.9	L	Vascular	203	Multiflex Ankle and Foot	bearing prosthesis suspension. All ankle feet complexes allowed for		
М	50	1.83	106.6	R	Vascular	175	Senator Freedom Foot [‡]	similar axial movement with the addition of specific differences		
М	41	1.92	1.92 95.4	R	Vascular	320	Multiflex Ankle and Foot	highlighted.		
М	70	1.74	96.7	R	Vascular	133	Multiflex Ankle and Foot			
(Mean ± SD)	56.1 ± 14.9	1.82 ± 0.08	91.7 ± 11.4			172 ± 72.2				

*Shock absorbing ankle foot complex, [‡]Energy returning ankle foot complex for low to moderately active participants. Within the study timeframe, participants attended 9.3 ± 4.6 appointments at the regional limb centre. These visits were due to; repairs and adjustments of the prosthesis accounted (42%); Consultant examinations (37%); Fitting and delivery of a prosthetic component (18%) and castings (3%).

Table 2. Group lead limb preferences and $\bar{x} \pm$ SD temporal-spatial, joint kinematic and foot marker displacement during obstacle crossing. Statistically

significant effects are highlighted in grey (p≤0.05). Positive values for joint kinematics indicate flexion/dorsiflexion.

One Month					Three Months				Six Months			
Lead Limb Preferences	Affected %	Intact %	Mean Number Trials		Affected %	Intact %	Mean Number Trials		Affected %	/o		n Number Trials
	31.2	68.8	6.5±1.0		38.3	61.7	8.1±2.5		41.8		58.2 7	′.6±1.4
								Main	Effects		Interaction E	ffects
			Limb	One Month	Three Months	Six Months	Time F	p	Limb F	p	Time*Lin F	
2 10 2 10 .	Walking velocity (m.s ⁻¹)		/ Lead Intact	0.72±0.15	0.93±0.19 0.85±0.19	0.89±0.20 0.89±0.20	(2, 17.48) = 1.97	0.17	(1, 17.04) = 0.30	0.59	(2, 15.65) = 1.01	0.39
	Stance duration (% gait cycle)		Lead Affected Lead Intact	66± 2.1	57±1.9 64±2.4	58±2.1 64±4.1	(2, 11.35) = 1.05	0.38	(1, 6.29) = 27.44	<0.01	(2, 14.96) = 0.54	0.59
			Trail Affected	69±5.1	61±2.5 68±3.4	60±2.4 68±4.0	(2, 9.03) = 1.51	0.27	(1, 4.98) = 37.78	<0.01	(2, 12.86) = 1.18	0.34
		rsiflexion during swing	Intact	7.39±0.47 4.63±3.49	6.48±2.07 11.45±7.47	5.30±3.27 18.00±8.42	(2, 9.19) = 1.36	0.30	(1, 6.19) = 2.35	0.18	(2, 13.26) = 3.73	0.05
0	Peak knee flexion	during loading respo	(°) Intact	18.28±3.06 24.74±6.73	16.22±6.38 17.63±4.40	13.77±4.69 19.20±9.81	(2, 16.73) = 1.29	0.30	(1, 13.96) = 5.32	0.04	(2, 12.28) = 0.84	0.46
Lead Limb	Peak kne	e flexion during swing	g (°) Affected Intact	78.14±0.38 98.08±10.01	74.31±10.45 91.26±8.26	73.40±10.59 91.14±15.32	(2, 9.67) = 0.05	0.95	(1, 5.30) = 8.35	0.03	(2, 11.64) = 0.75	0.49
	Knee F	ROM across gait cycle	e (°) Affected Intact	70.66±2.21 89.15±12.36	64.13±11.16 87.93±10.72	68.06±6.96 86.43±15.01	(2, 10.07) = 0.18	0.84	(1, 3.31) = 11.95	0.04	(2, 11.20) = 0.19	0.83
	Peak hi	p flexion during swing	g (°) Affected Intact	62.37±6.31 60.58±5.48	56.16±5.17 51.70±7.69	58.70±8.41 58.19±12.95	(2, 16.15) = 2.84	0.09	(1, 15.24) = 0.25	0.62	(2, 13.06) = 0.45	0.65
	Hip F	ROM across gait cycle	e (°) Affected Intact	62.46±6.19 63.74±6.00	60.31±2.44 60.10±6.06	60.52±6.10 62.96±6.92	(2, 8.87) = 1.62	0.25	(1, 5.29) = 0.14	0.72	(2, 11.87) = 0.11	0.90
Trail Limb	Peak ankle do	rsiflexion during swing	g (°) Affected Intact	10.68±2.65 15.45±12.51	6.82±2.69 15.32±8.42	5.58±3.67 16.60±5.22	(2, 12.38) = 0.58	0.57	(1, 10.34) = 16.42	<0.01	(2, 14.64) = 0.44	0.65
	Peak knee flexion	during loading respo	onse Affected (º) Intact	18.38±13.23 18.75±0.62	16.94±7.14 18.78±2.60	14.70±5.15 20.38±8.77	(2, 10.63) = 0.06	0.94	(1, 9.73) = 1.52	0.25	(2, 14.13) = 0.46	0.64
	Peak kne	e flexion during swing	g (°) Affected Intact	87.96±3.03 94.65±6.50	84.94±15.86 92.75±9.78	82.60±15.85 95.88±16.81	(2, 9.05) = 0.28	0.76	(1, 5.40) = 1.69	0.25	(2, 11.59) = 0.97	0.41
	Knee F	ROM across gait cycle		81.46±7.69 93.43±16.99		81.53±17.42 92.74±15.51	(2, 9.18) = 0.28	0.76	(1, 5.27) = 1.88	0.23	(2, 11.59) = 0/08	0.94
-	Peak hi	p flexion during swing	g (°) Affected Intact	36.98±10.95 46.45±2.64	38.98±9.09	39.04±11.63 45.63±14.17	(2, 10.65) = 0.20	0.82	(1, 11.07) = 1.02	0.33	(2, 13.40) = 0.86	0.45
	Hip F	ROM across gait cycle	e (°) Affected Intact	45.60±1.52 46.60±1.07	45.87±7.08 46.66±5.93	43.61±9.38 46.62±5.53	(2, 5.99) = 0.93	0.45	(1, 2.32) = 0.03	0.89	(2, 9.96) = 0.14	0.87

Table 3. Statistical analysis of group \bar{x} load and decay rates, peak ground reaction forces (GRF) and peak joint powers of the lead limb and trail

limb during obstacle crossing. Statistically significant effects are highlighted in grey (p≤0.05).

			Interaction Effects					
	Variable	Time		Limb		Time*Limb		
		F	р	F	р	F	р	
	Load Rate	(2, 9.04) = 0.23	0.80	(1, 9.95) = 4.81	0.05	(2, 9.72) = 0.07	0.94	
	Decay Rate	(2, 7.96) = 4.43	0.05	(1, 8.21) = 0.61	0.46	(2, 7.48) = 0.50	0.63	
	Vertical GRF Fz1	(2, 12.74) = 0.18	0.84	(1, 10.39) = 0.20	0.66	(2, 12.84) = 0.09	0.92	
	Vertical GRF Fz2	(2, 5.63) = 5.29	0.05	(1, 5.98) = 7.43	0.03	(2, 6.06) = 1.23	0.36	
~	(A1) Ankle power absorption during stance	(2, 4.14) = 0.18	0.85	(1, 7.36) = 2.29	0.17	(2, 11.90) = 0.03	0.97	
ц Д	(A2) Ankle power generation during pre-swing	(2, 12.98) = 0.01	0.99	(1, 14.09) = 8.00	0.01	(2, 11.07) = 0.83	0.46	
	(K1) Knee power absorption during loading response	(2, 6.27) = 0.08	0.92	(1, 13.43) = 0.75	0.40	(2, 8.20) = 0.16	0.86	
ad	(K2) Knee power generation during mid-stance	(2, 8.46) = 1.43	0.29	(1, 6.95) = 0.47	0.51	(2, 10.36) = 0.01	0.95	
Lead Limb	(K3) Knee power absorption during pre-swing	(2, 11.88) = 2.45	0.13	(1, 12.74) = 4.89	0.05	(2, 10.44) = 0.83	0.46	
_	(K4) Knee power absorption during terminal swing	(2, 10.94) = 0.15	0.87	(1, 14.27) = 9.26	0.01	(2, 12.90) = 0.49	0.63	
	(H1) Hip Power generation during loading response	(2, 14.68) = 0.37	0.70	(1, 15.31) = 1.71	0.21	(2, 12.58) = 0.82	0.46	
	(H2) Hip power absorption during stance	(2, 12.38) = 0.51	0.61	(1, 13.61) = 0.13	0.72	(2, 10.35) = 1.51	0.27	
	(H3) Hip power generation during pre-swing	(2, 9.45) = 0.06	0.94	(1, 10.75) = 4.85	0.05	(2, 11.19) = 0.08	0.92	
	Load Rate	(2, 4.86) = 0.80	0.50	(1, 3.12) = 3.56	0.15	(2, 7.14) = 0.06	0.95	
	Decay Rate	(2, 4.75) = 2.29	0.20	(1, 1.90) = 0.44	0.58	(2, 6.80) = 4.54	0.06	
	Vertical GRF Fz1	(2, 4.09) = 0.62	0.58	(1, 2.08) = 1.47	0.35	(2, 6.90) = 2.76	0.13	
	Vertical GRF Fz2	(2, 5.73) = 2.30	0.19	(1, 3.14) = 8.86	0.06	(2, 7.43) = 2.22	0.18	
0	(A1) Ankle power absorption during stance	(2, 5.13) = 10.12	0.02	(1, 2.45) = 5.06	0.13	(2, 7.38) = 6.43	0.02	
Trail Limb	(A2) Ankle power generation during pre-swing	(2, 4.40) = 6.22	0.05	(1, 2.65) = 28.29	0.02	(2, 6.15) = 3.08	0.12	
	(K1) Knee power absorption during loading response	(2, 5.71) = 5.62	0.05	(1, 3.17) = 11.49	0.04	(2, 5.86) = 2.51	0.16	
ail	(K2) Knee power generation during mid-stance	(2, 9.42) = 1.99	0.19	(1, 7.49) = 9.73	0.02	(2, 6.61) = 0.16	0.85	
μ	(K3) Knee power absorption during pre-swing	(2, 3.91) = 7.72	0.04	(1, 0.81) = 8.48	0.26	(2, 5.20) = 1.14	0.39	
	(K4) Knee power absorption during terminal swing	(2, 7.19) = 2.01	0.20	(1, 4.55) = 21.99	0.01	(2, 6.04) = 1.82	0.24	
	(H1) Hip power generation during loading response	(2, 10.19) = 1.02	0.39	(1, 8.39) = 0.44	0.53	(2, 7.60) = 0.46	0.65	
	(H2) Hip power absorption during stance	(2, 7.50) = 0.42	0.67	(1, 6.09) = 0.31	0.60	(2, 5.18) = 2.54	0.17	
	(H3) Hip power generation during pre-swing	(2, 8.52) = 0.52	0.61	(1, 7.09) = 0.09	0.78	(2, 6.19) = 0.18	0.84	