



The influence of moisture on ash strength: implications for understanding volcanic stratigraphy

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Abstract

Ash layers within extensive pyroclastic density current (PDC) deposits can be important in understanding the evolution of explosive eruptions. If interpreted as ashfall deposits, they may be used to identify hiatus episodes and determine how many pyroclastic density currents were generated during an eruption. However, such layers, which often contain ash aggregates indicating the presence of moisture, may be variably deposited, preserved and eroded, and there has been little study of their characteristics. This paper investigates the geomechanical properties of ash layers through a comparison of field observations and experimental analysis. We present new field evidence of intriguing relationships between ash aggregate layers and overlying ignimbrite facies within the 273 ka Poris ignimbrite of Tenerife. We identify three types of interactions, each displaying distinct erosional and remobilisation behaviours associated with varying moisture conditions. To complement these field observations, we performed direct shear box, ring shear and drop tests under both low (1 wt.%) and high (> 15 wt.%) moisture conditions. We find that fine pyroclastic material increases yield strength with moisture compared to dry conditions. Furthermore, we see shear thickening behaviours in fine ash at high moisture content. These behaviours show how ash layers formed under low and high moisture conditions are more likely to be preserved than dry layers. This may lead to misunderstanding in flow unit interpretation and, therefore, assessments of eruption frequency. Furthermore, dry, loose ash material may promote flow bulking, increasing mobility, runout and flow velocities in PDCs.

Keywords Erosion · Entrainment · Remobilisation · Cohesion · Substrate · Sedimentary structures

Introduction

Pyroclastic density currents (PDCs) are a deadly volcanic hazard that can form during column, lava dome collapse, or lateral blast events (Fisher 1979; Branney and Kokelaar 2002) and pose a significant hazard to communities living around PDC-forming volcanoes (Auker et al. 2013; Lube et al. 2020). PDC activity can be short-lived (seconds to minutes) when associated with lava dome collapse, for example, or can be long-lived and sustained (hours to days) when associated with large-magnitude, caldera-forming eruptions (Fisher 1979; Branney and Kokelaar 2002; Brown et al. 2003; Sulpizio et al. 2014; Lowe and Pittari 2021).

The nature of PDC activity can be determined through visual observation (e.g., Cole et al. 1998) and field study of the resultant pyroclastic material, known as ignimbrite, deposited as these currents move across the landscape (e.g., Fisher 1979). Analysis of ignimbrite stratigraphy has been vital in interpreting the evolution of historic PDC events

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(e.g., Sigurdsson et al. 1984; Cas and Wright 1987; Druitt et al. 1989; Wilson 1993; Brown and Branney 2004; Lucchi et al. 2018; Dowey and Williams 2022), with stratigraphic data collection informing hazard planning strategies for future eruptions. Flow unit identification (i.e., how many PDCs formed within a single event) may form an essential part of this analysis (e.g., Silva Parejas et al. 2010; Brown and Branney 2013; Douillet et al. 2013; Smith and Kokelaar 2013; Cavazos-Álvarez et al. 2020; Dowey et al. 2024).

A flow unit is best defined as a stratigraphic package of ignimbrite that records the passage of an individual PDC (i.e., one flow unit = one PDC) (Sparks 1976). In a model of progressive aggradation of ignimbrite material (Branney and Kokelaar 2002), flow units are separated by evidence of hiatus where no PDC activity is present in that area at that time. Hiatus layers may be represented by pumice or ash fallout layers, which can represent a change in eruption processes (i.e., during the same eruption), or by evidence of secondary reworking or soil horizons within an ignimbrite sequence which represents a longer time pause or separate eruptions (e.g., Sparks et al. 1973; Sparks and Walker 1977; Wright and Walker 1981; Sigurdsson and Carey 1989; Branney and Kokelaar 1992; Pittari et al. 2006; Brown and Branney 2013; Cavazos-Álvarez & Carrasco-Núñez 2019). Ash fall layers (Fig. 1) can become recorded in an ignimbrite succession during hiatuses in PDC activity either by deposition from the co-ignimbrite plume (i.e., the ash-laden cloud that lofts above a PDC, e.g., Brown and Branney 2004) or from the eruption plume (Brown et al. 2003).

In significant, sustained eruptions, PDC activity can be unsteady through time, displaying phases of waxing and waning due to factors such as changing mass flux at source (Fig. 1) (Pittari et al. 2006; Báez et al. 2020; Charbonnier et al. 2023). Such unsteadiness can cause temporal changes in PDC mobility and run out, both longitudinally away from, and laterally around a volcano (e.g., Williams et al. 2014) and may lead to variable preservation, erosion, or remobilisation of key hiatus indicators such as ash fall layers (e.g., Dowey et al. 2024) (Fig. 2). Such factors can contribute to spatial complexity in the record of hiatus and, therefore, of flow units, leading to contradictory interpretations of eruption history at different locations (Dowey et al. 2024). Understanding the potential for erosion or preservation of these distinct ash layers under various conditions is vital to understanding volcanic sequences, eruption evolution, and hazard identification.

Changes in variables: flow and deposit

Whether a PDC forms a deposit, erodes the substrate or bypasses an area depends on several factors. Eruption dynamics, such as mass flux and unsteadiness, can vary throughout the lifespan of the current (Bursik and Woods 1996; Pittari

et al. 2006; Rowley et al. 2023). Similarly, local environmental conditions play a crucial role in flow behaviours, including surface roughness and topography (Sparks et al. 1997; Brand et al. 2014). These factors influence the fundamental characteristics of the overriding current, such as thickness, particle concentration, pore pressure (Roche et al. 2013) and the resulting conditions at the flow boundary zone at the base of the PDC, which govern the depositional, erosional, or bypassing regime (Brown and Branney 2004; Branney and Kokelaar 2002).

Under depositional or bypassing conditions, an ash layer is more likely to be preserved, whereas erosional conditions may lead to its removal (Brown and Branney 2004). Erosion occurs where erosive forces exceed the resistive forces within the ash material, which include gravity, friction, cohesion, and adhesion (Grabowski et al. 2011). Several factors can influence these forces, such as particle size distribution (Alias et al. 2014), material composition, density, fines content (Jiang et al. 2015; Walding et al. *in press*), and moisture content (Liu et al. 2022; Walding et al. 2023, *in press*).

Moisture can be introduced into a PDC from various sources, including pre-eruptive groundwater conditions, surface water interaction and atmospheric humidity (Self and Sparks 1978; Moyer and Swanson 1987; Darteville et al. 2002; Cole et al. 2002; Hurwitz et al. 2003; Brown and Branney 2013; Houghton et al. 2015; Pepin et al. 2017; Camuffo 2019; Vecino et al. 2022; Shimizu et al. 2023). Furthermore, post-depositional factors like the extent and type of compaction (e.g., diagenesis) and additional water content (i.e., rainfall) will also contribute to the overall final strength of the ash material (Kim and Sture 2008; Chen et al. 2021a, b; Walding et al. 2023, *in press*).

This work and aim

In this work, we investigate the controlling factors governing the strength of fine-grained pyroclastic materials to inform understanding of the fate of ash layer substrates during sustained PDC events. We analyse striking lithostratigraphic relationships observed in moist ash layers on Tenerife where moisture content is inferred by the presence of moisture-induced ash aggregations (Brown et al. 2010, 2012) and hypothesise that the preservation of ash layers depends on their strength, which can be controlled by moisture. The strength behaviours of various pyroclastic ash materials under different moisture conditions, ranging from 1 to 70 wt.%, have been investigated in laboratory tests to better understand these observations. This multidisciplinary work, which brings together volcanic stratigraphers and engineering geologists, aims to quantify the behaviour of volcanic ash in “dry” and “wet” shear environments. These relationships may have significant implications for the preservation or erosion of deposit architecture.

Flow unit formation in a sustained current: Ash hiatus layer

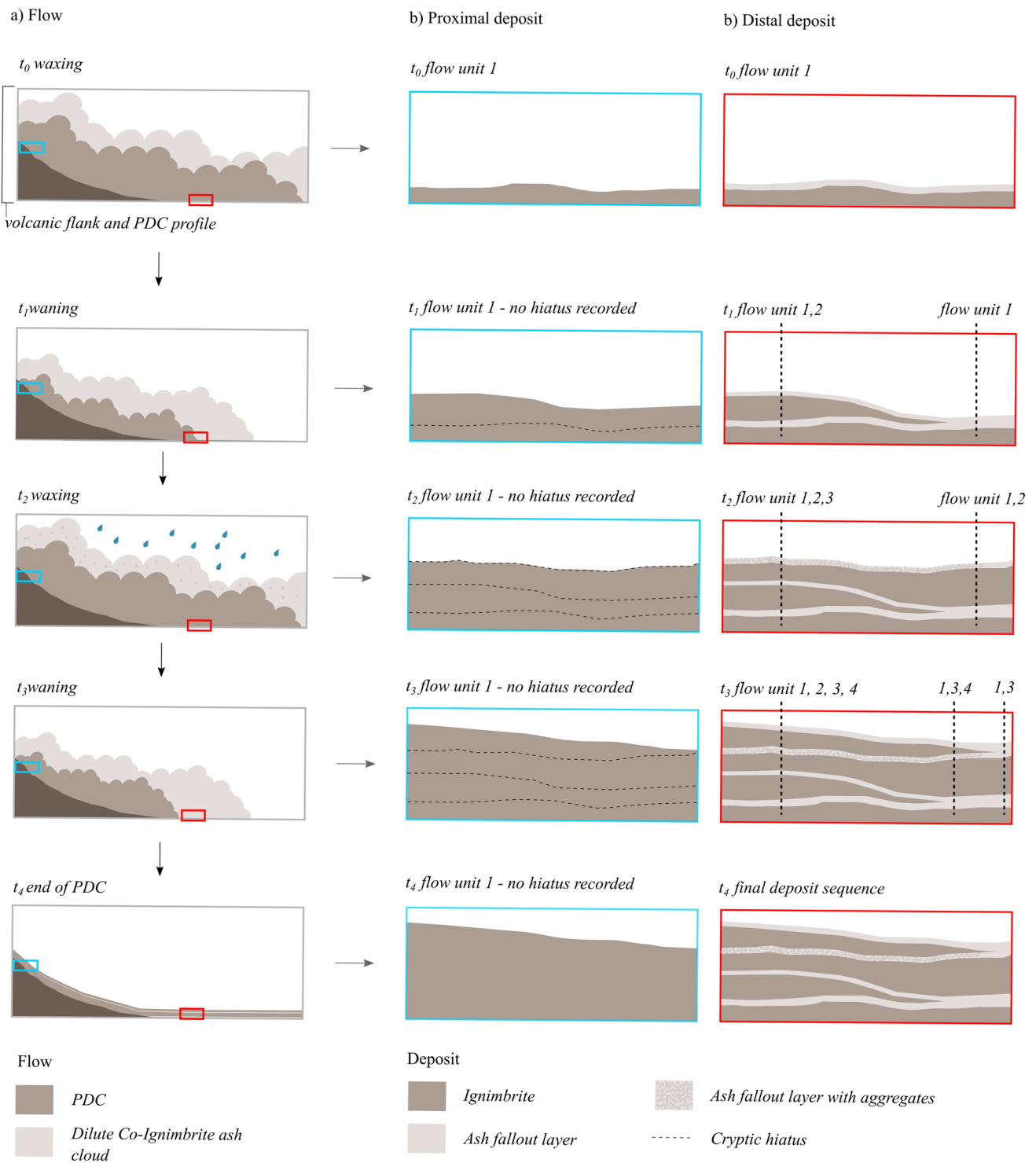


Fig. 1 Conceptual model depicting how variable deposition of ash fallout layers in proximal and distal locations during unsteady PDC activity can complicate interpretations of flow units and eruption history. As a single PDC undergoes waxing and waning through time and, therefore, changes in run out through time (column a, t_0 – t_4), co-ignimbrite ash is deposited during episodes of local hiatus. Dis-

tally (column c), the final deposit may appear to have multiple ‘flow units’ (dashed line), but only one unsteady PDC was active throughout. Proximally (column b), no evidence of hiatus or ‘flow-units’ are evident (model based on field correlations presented in Dowe et al. 2024)

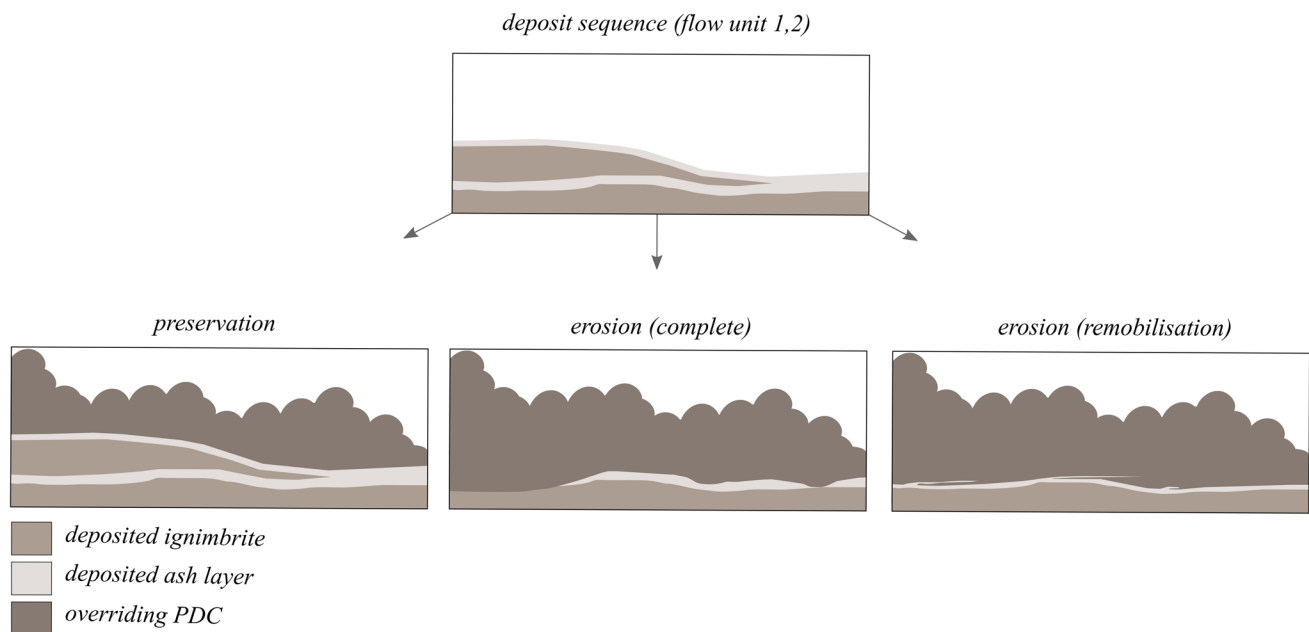


Fig. 2 Illustration to show how ash layers recording hiatus in an ignimbrite succession may be (a) preserved, (b) eroded, or (c) remobilised by subsequent PDC activity, either due to waxing of a sustained

unsteady current or by renewed activity following a complete cessation in PDC activity

Terminology, materials and methods

Fieldwork terminology

Volcanic ash (pyroclastic material with a particle diameter of < 2 mm, Cas, and Wright 1987) is a fine granular material, and the finest fractions (< 0.064 mm) can be considered a powder. Grain size controls a variety of changes in the mechanics of how these materials behave, and for this work the more cohesive behaviour of fine powder materials is particularly relevant (Geldart 1973).

Ash aggregates are clusters of volcanic ash particles formed via contact or interstitial forces. They can form due to electrostatic interaction and are found to be prevalent in moisture-influenced conditions (i.e., forming in the presence of rain or high-moisture environments) (Reimer 1983; Gilbert and Lane 1994; Schumacher and Schmincke 1995; Brown et al. 2012; Telling et al. 2013; Diaz-Vecino et al. 2023). Ash aggregates have a higher terminal fall velocity than “dry” ash fallout, due to them being greater in size. They can be found in the ash fall deposits of co-ignimbrite clouds or from plume fallout that records hiatus between distinct episodes of PDC activity (Sparks et al. 1973; Sigurdsson and Carey 1989; Brown and Branney 2004; Pittari et al. 2006; Brown et al. 2010; Dowey et al. 2024).

In this study, we use the term “ash pellet” (AP1 in Brown et al. 2012 scheme) to refer to unstructured ash aggregates that are clast supported and “accretionary lapilli” (AP2 in Brown et al. 2012 scheme) to refer to structured, whole and

fragmented ash aggregates that are matrix supported (Supplementary Material A). Both accretionary lapilli and ash pellets can also be formed in central eruption plumes, as well as co-ignimbrite clouds (Brown et al. 2012). On Tenerife, layers of unstructured ash pellets are interpreted to form within moist co-ignimbrite clouds, where ash begins to agglomerate as moisture condenses (Brown et al. 2010). Structured accretionary lapilli with multiple concentric layers have been interpreted to record vertical movement in a PDC system. For example, as accretionary lapilli are lofted and cycled in the thermally stratified area of a PDC, repeating layers of cohesive ash are accreted before lapilli return to relatively drier and hotter zones of the current (Brown et al. 2010). In the context of this work, ash pellets are moist on deposition, and accretionary lapilli are dry and brittle (as evidenced by fragmentation in some cases, Brown et al. 2010).

Fieldwork stratigraphy and lithofacies

Sedimentological analysis (logging, detailed imaging and sampling) of flow-unit ash layer marker beds and their contacts with overriding deposits was carried out in the Bandas del Sur region of Tenerife (March 2023). Lithostratigraphic features and physical relationships of selected ash layers of the 273 Ka Poris eruption, Tenerife, are reported. The outcrops are located in the Poris Quarry [GR: 2,810,696, 01627001] and Montana Magua [GR: 2,811,244, 01626702] (Figs. 3a.ii, 4a.iii, 5a.ii and 6a.ii). The stratigraphy in these

locations has been worked on extensively by others (Edgar et al. 2002, 2007; Brown et al. 2003; Brown and Branney 2004; 2013). The ash pellet layers investigated here are very-fine- to fine-grained, buff-coloured ash and have been previously interpreted to record local hiatus in PDC activity (Brown and Branney 2004, 2013). Where accretionary lapilli are present, this represents the lofting of pellets in the body of the PDC prior to deposition (Brown and Branney 2004). Lithofacies analysis is based on the approach and descriptions of Branney and Kokelaar (2002), see Supplementary Material B.

Experimental materials

Through direct shear, ring shear and drop test geomechanical experiments, the properties of a range of fine pyroclastic material at dry, low (1 wt.%) and high (> 15 wt.%) moisture content were explored.

Material selection

The pyroclastic material studied in the field in Tenerife is lithified and could not be utilised as a loose granular material in laboratory work. Our experiments instead used a suite of fine pyroclastic-ash material from a range of volcanoes (Table 1). Materials < 2 mm were used due to the size restrictions imposed by the shear equipment. The materials were chosen purposefully to span a range of particle sizes, sorting, particle ranges, fines content, composition, and shape characteristics to explore the effect of these variables on moisture and shearing behaviours (Table 2). The materials chosen have been previously described by Walding et al. (2023 and in press). Cornstarch (5–340 µm) was also used as a comparative non-Newtonian synthetic material.

Material characteristics

Particle size analysis using a CAMSIZER X2 (University of Bristol) was completed to establish the shape and size characteristics of the dry material, with a maximum resolution of 0.8 µm per pixel. Particle size characteristics were measured before and after shear experiments to document physical changes, such as particle crushing.

Sphericity (SPHT) was calculated using Eq. 1, where P is the measured circumference of the particle, and A_p is the area covered by particle projection (see Table 2). An ideal sphere would record SPHT as a value of 1 (Liu et al. 2015).

$$\text{SPHT} = \frac{4\pi A_p}{P^2} \quad (1)$$

Symmetry, which describes the even distribution of the particle around the centre line, was calculated using

Eq. 2, where r_1 and r_2 are minimum and maximum particle radii (Buckland et al. 2021). Symmetrical particles will have a symmetry value of 1, and asymmetrical particles < 1.

$$\frac{1}{2} \left[1 + \min \left(\frac{r_1}{r_2} \right) \right] \quad (2)$$

The particle size data were processed using GRADISTAT (Blott and Pye 2001) to derive particle characteristics using the moments methods (Inman 1952) to calculate logarithmic and geometric mean ($(\bar{x}) \emptyset$), median (\emptyset), range (µm), sorting index ($(\sigma) \emptyset$), sorting (σG), skewness ($(Sk) \emptyset$), kurtosis ($(K) \emptyset$), and the geometric mean (µm). Following the approach outlined in Breard et al. (2019), we calculated the D_{32} (mm) and fines content (< 63 µm, %) of the material. D_{32} values, also known as the surface-weighted mean diameter can characterise material fluidisation behaviour (Breard et al. 2019).

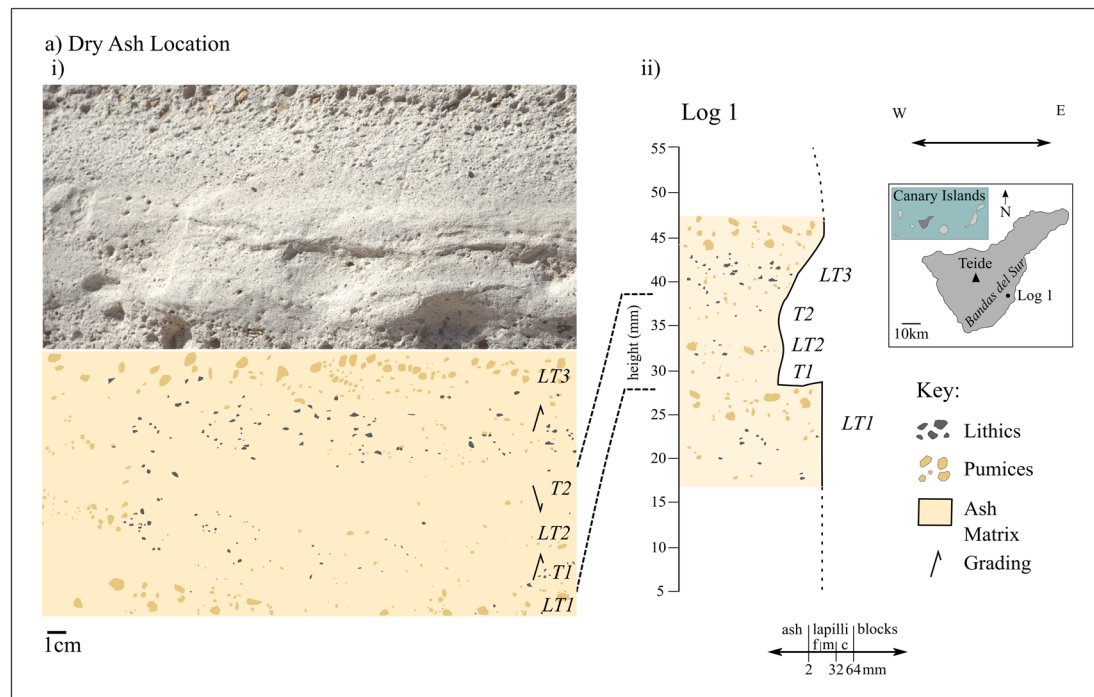
$$D_{32}(\text{mm}) = 2 - \left[\mu_{\text{PSD}}(\Phi) + \frac{\ln^2}{2} \sigma_{\text{PSD}}^2(\Phi) \right] \quad (3)$$

where μ_{PSD} and σ_{PSD} are the mean and standard deviation (Eq. 3, Breard et al. in Φ units, 2019).

Experimental methods

We describe material properties using peak and yield stress, bulk and shear modulus (Sheng et al. 2011; Donaldson et al. 2013; Keaton 2018). Yield stress describes the point at which a material transitions from elastic to plastic behaviour. Elastic deformation describes reversible stretching or compression, where materials with higher elastic moduli are more resistant to deformation. Plastic deformation is irreversible, and the material will continue to deform until it fails at peak stress (i.e., the maximum stress before failure). Therefore, the yield stress measures a material's ability to withstand deformation without failing and, therefore, how less or more likely the material is to move. Similarly, bulk modulus describes the resistance of a material to changes in volume from hydrostatic stress (Donaldson et al. 2013), and shear modulus describes the resistance of a material to shear deformation (Keaton 2018).

We investigated variation in yield strength, bulk and shear modulus using direct and ring shear apparatus at low (1 wt.%) and high moisture (> 15 wt.%) contents (Supplementary Material C). Variations were then explored using the bulk modulus of material at high moisture, with drop test experiments to explore further shear thickening (i.e., non-Newtonian) or shear thinning (i.e., Newtonian) behaviours (Supplementary Material C).



b) "dry" veneer ignimbrite deposit formation from a PDC

waxing and waning results in changes in current behaviour and resulting lithofacies throughout time

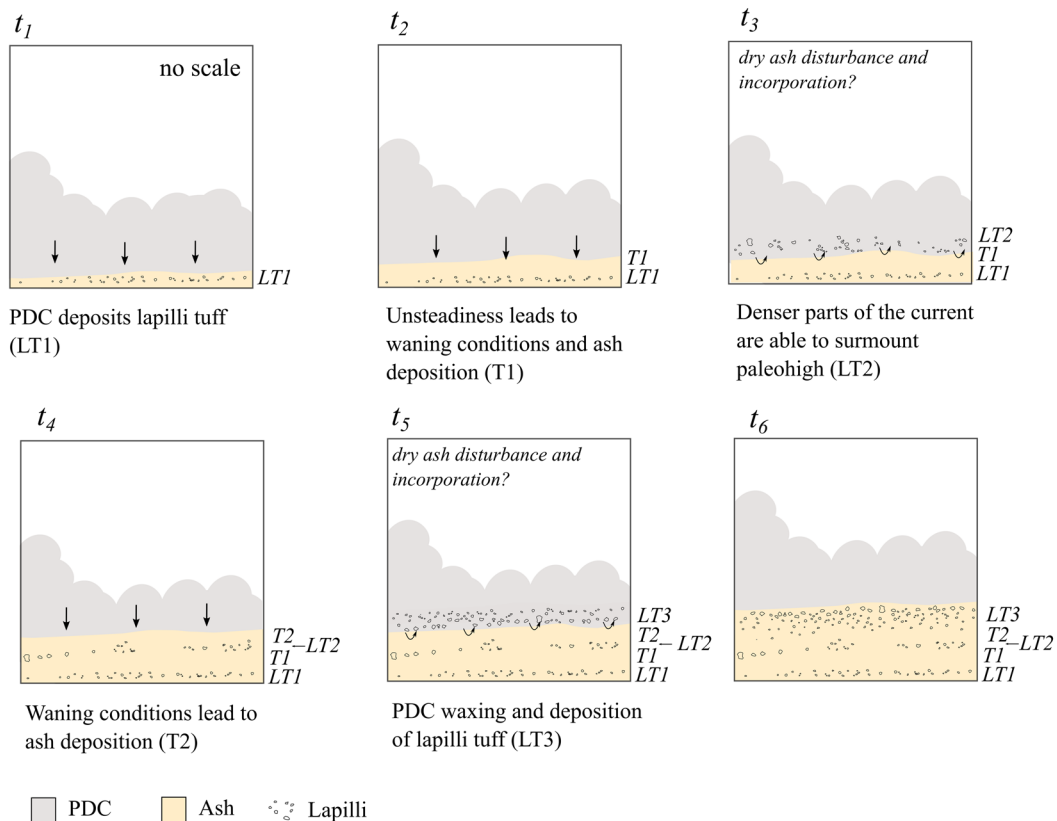


Fig. 3 **a.i** Ash-rich lapilli-tuff (LT1, LT2 and LT3) in contact with tuff (T1 and T2) within the Cueva Honda member of the Poris Formation at Montaña Magua. **a.ii** Location map, log at GR: 2,811,282, 01626695. See lithofacies terminology in Supplementary Material B. **b** Interpretation of the formation of deposits shown in Log 1 through time (t) (see text for explanation)

Direct shear

Direct shear tests (Supplementary Material C, e.g., Niroumand 2017) were performed to determine the shear strength of pyroclastic materials with the addition of moisture. These were completed using the direct shear apparatus (Faculty of Engineering, University of Bristol). Three experiments were undertaken on 200 g of various materials (Tung 1, Tung 4, Tung 5 and Colima) at 0, 0.25, 0.50, 1 and 5 wt.% moisture. Samples were dried at 80 °C for 24 h before the experiments to ensure the removal of adsorbed moisture. Agglomerations were broken up by sieving before the addition of water. On addition of moisture, the samples were thoroughly mixed to ensure an even moisture distribution.

For each experiment, the material was loaded into the shear cell (60 × 60 mm) and consolidated for 20 min prior to shearing. The consolidation and shear tests were completed under a normal stress of 1, 14 and 27 kPa. These normal stress values were chosen to encompass a range of loads and to ensure behaviours were seen in a dry and wet (by adding moisture) state without generating pore pressure. The shear test was then completed at a 1 mm/min rate until peak shear was reached or the shear box length limited completion. Experiments were also completed at 0.5 mm/min to ensure we were not seeing significant influence from pore pressure. The results from the 0.5 mm/min tests are reported in Supplementary Material D and show similar results to that of the 1 mm/min tests. Therefore, we can conclude that pore-pressure is not being generated by higher shear rates, so is not affecting our results.

Ring shear

A suite of fine pyroclastic material (< 1 mm) with varying moisture contents was tested in the Imperial College Ring Shear apparatus (Supplementary Material C, Bishop et al. 1971) at the University of Leeds, in order to inform interpretations of PDC behaviours made from stratigraphic relationships in Tenerife. Brown Tuff, Atitlan 2 and Taupo 1 (Table 2) samples were used for ring shear testing, to represent fine ash materials with high fines content. The samples were prepared as in the direct shear box tests.

The ring shear comprises two split confining rings with an outer diameter of 152.4 mm and an inner of 101.6 mm (Supplementary Material C). The depth of the sample area is 19 mm. Around 150–200 g of samples were used to run each

experiment; variations in sample weight were due to changes in the density of the material and the required amount to fill the chamber. Each material was weighed before and after loading the shear chamber. The samples were sieved and sheared initially when dry (0 wt.% moisture). The initial set of experiments records the consolidation of the sample under a varying normal weight load. The second set of experiments records the shear behaviour of the samples. We then introduced water (0.5 and 1 wt.%) into the sample and repeated the experiment. Due to time constraints, higher moisture contents were not tested.

The ring shear tests were performed at constant normal stresses of 5, 10 and 20 kPa for each water addition. For each experiment, consolidation and shear measurements were recorded every 1 s for the first hour, then every minute for an hour and finally every half-hour for the remainder of the experiment. Shearing was completed at a shear rate of 1.0 deg/min. The relative horizontal shear and vertical displacement were recorded, with the latter being measured through compaction or dilation of the material. It should be noted that the right proving ring sensor had fluctuating background noise that resulted in noisy results. This was reduced by using a moving average of the results.

The Mohr–Coulomb failure criterion describes the failure of materials where peak shear stress values are determined by cohesion and internal friction angle (Massoudi and Mehrabadi 2001). Using the Mohr–Coulomb failure criterion on the normal stress and peak stress values, we determined friction angle (the ability of a material to withstand shear stress, therefore, higher resistance to erosion), cohesion and dilation (i.e., shear thickening) and compaction (i.e., shear thinning).

Drop test

The drop test (Supplementary Material C, Crawford et al. 2013) was conducted on the Atitlan 1, Colima, Taupo 1, Taupo 2 and Tung 6 pyroclastic materials at varying states of high-water addition to explore the effects of shear thickening and thinning behaviours. Cornstarch and water (also named Oobleck), saturated at 75 wt.% moisture was used as a comparison sample to show explicit shear thickening behaviours.

A steel ball (20 mm diameter, 7910 kg/m³) was dropped from a height of 270 mm onto loose material saturated at 0, 15, 25, 30, 40, 50, 60, 70 and 90 wt.% in a clear box (60 × 60 × 60 mm). Each experiment was completed three times. Video footage (700 fps), using a high-speed camera (Phantom VEO 440), recorded the steel ball hitting the sample. The footage was then analysed using ImageJ (Schindelin et al. 2012) to observe the nature of the interaction of the falling ball with the material deposit (i.e., the ball sinking through the deposit or the ball bouncing off the deposit). After each experiment, the ball penetration depth (i.e., how

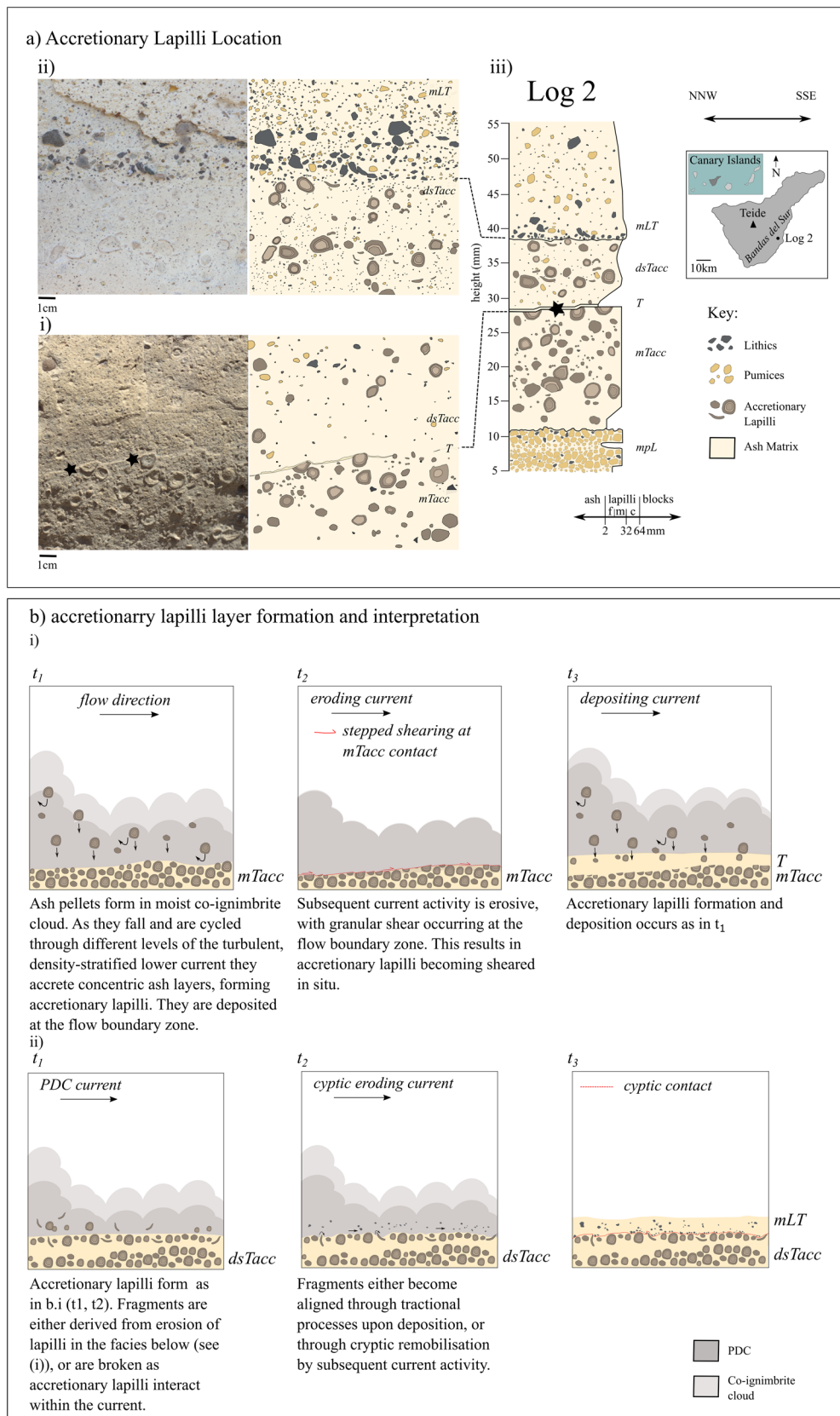


Fig. 4 **a.i** Accretionary lapilli layer (mTacc) in contact with overlying thin tuff (T) layer, observed in the Magua Member of the Poris Formation at Montaña Magua [GR: 2,811,244, 01626702]. Accretionary lapilli are sheared at the contact (star). **a.ii** Diffuse stratified accretionary lapilli unit (dsTacc) in contact with overlying lapilli-tuff layer (mLT). Accretionary lapilli are fragmented at the contact. **a.iii** Location map, log at GR: 2,811,244, 01626702. See lithofacies terminology in Supplementary Material B. **b** Interpretation of formation of **i** the lower contact (4a.i) showing granular shear occurring at the flow boundary zone in log 2, and **ii** the more cryptic upper contact shown in log 2 (see text for full explanation)

far the ball made it through the deposit) was measured to gain insight into the material's resistance under varying moisture.

Variations in ash layer strength on Tenerife

“Dry” ash layer contact

At the Montaña Magua location on Tenerife (Fig. 3a), two contacts between ash (T) and lapilli-tuff (LT) occur within the Cueva Honda member (< 0.90 m thick, distributed from La Caleta to Montaña Magua) of the Poris Formation (flow unit 3, member 7, Brown and Branney 2004, 2013).

At this location, ash layers (T1 and T2) occur between lapilli-tuff lithofacies (LT1, LT2, LT3). The contact between lapilli tuff (LT1) and tuff (T1) is typically clear and well-defined, whilst the upper contact between the tuff (T2) and lapilli tuff (LT3) is more graduated and diffuse, occasionally displaying grading. The ash layers (T1 and T2) are well sorted and normally graded into lapilli tuff. The second lapilli tuff layer (LT2, sandwiched between T1 and T2) contains pumice, lithics, and some eroded remnants of sub-rounded pumice clasts and shows no sign of ash aggregates (Fig. 3a).

Interpretation

This ash layer is interpreted to be an ignimbrite veneer, which is a thin ignimbrite layer deposited by dilute parts of a PDC that can surmount topographic palaeohighs (Branney and Kokelaar 2002; Brown and Branney 2004; flow unit 3, member 6, Brown and Branney 2013). The lack of ash aggregates indicates formation in low-humidity or high-temperature environments with little external influence of moisture (such as precipitation or steam).

Transitions from lapilli tuff to ash, and then back to lapilli tuff, reflect unsteadiness in PDC dynamics (and therefore changes in flow boundary zone conditions) through time (t1–t5, Fig. 3b). Waxing or waning energy in the system may have led to the varying ability of denser parts of the current to surmount topography. The diffuse and graded nature of

the contact, together with evidence that these ash layers were dry and likely loose on deposition, makes it seem likely that the ash layers were disturbed, remobilised and potentially incorporated into subsequent lapilli tuff layers as they were deposited (t3 and t5).

Sheared accretionary lapilli ash layer contact

Two subtle, cryptic contacts were identified at Montaña Magua, at different stratigraphic levels within the Magua Member (< 15 m thick, flow unit 3, Member 6 in Brown and Branney 2004) of the Poris Formation (Fig. 4). At this location, the Magua Member consists of a fine-grained tuff containing scattered accretionary lapilli ranging from 3 to 30 mm in size (Brown and Branney 2004; Brown et al. 2003; Brown et al. 2010).

The first contact occurs between an accretionary lapilli-rich ash layer (mTacc in Fig. 4a.i) and a < 3 mm thick tuff layer above (T), which is then overlain by a diffusely stratified accretionary lapilli layer (dsTacc). In the lower aggregate-rich layer (mTacc), accretionary lapilli are mostly intact and unfragmented; however at the contact with the tuff, which is irregular with an undulating or stepped appearance (Fig. 4a.i), accretionary lapilli are sheared in situ.

The overlying diffusely stratified accretionary lapilli facies (dsTacc) contains vertical transitions from increased to decreased accretionary lapilli concentrations. The second distinct contact, between this facies and massive lapilli tuff (mLT) above, is marked by a difference in lithic content (Fig. 4a.ii). In the diffusely stratified facies (dsTacc), accretionary lapilli are mostly intact, although occasional angular accretionary lapilli fragments (< 20 mm) appear aligned with flow direction. In some areas, ash at the base of the massive lapilli facies (mLT) appears to be draped over whole accretionary lapilli, with no evidence of shear or erosion.

Interpretation

The lower contact between the accretionary lapilli (mTacc) and ash layer (T) is sharp and stepped and is interpreted to have formed through abrasion during low-impact granular shear in the lower regions of the current (Fig. 4b.i, Branney and Kokelaar 2002; Brown et al. 2010). This observation is significant because layers rich in accretionary lapilli are thought to form during fluctuating current intensity (waxing and waning), perhaps making them unlikely to be fully cemented during the brief deposition period (Brown et al. 2010). However, in this example, the resistance of the accretionary lapilli to plucking from the substrate, the lack of disaggregation, and the planar erosion (shearing) through some of the lapilli suggest that both the accretionary lapilli (mTacc) and the ash (T) layer in which they were deposited had considerable strength. This strength during deposition

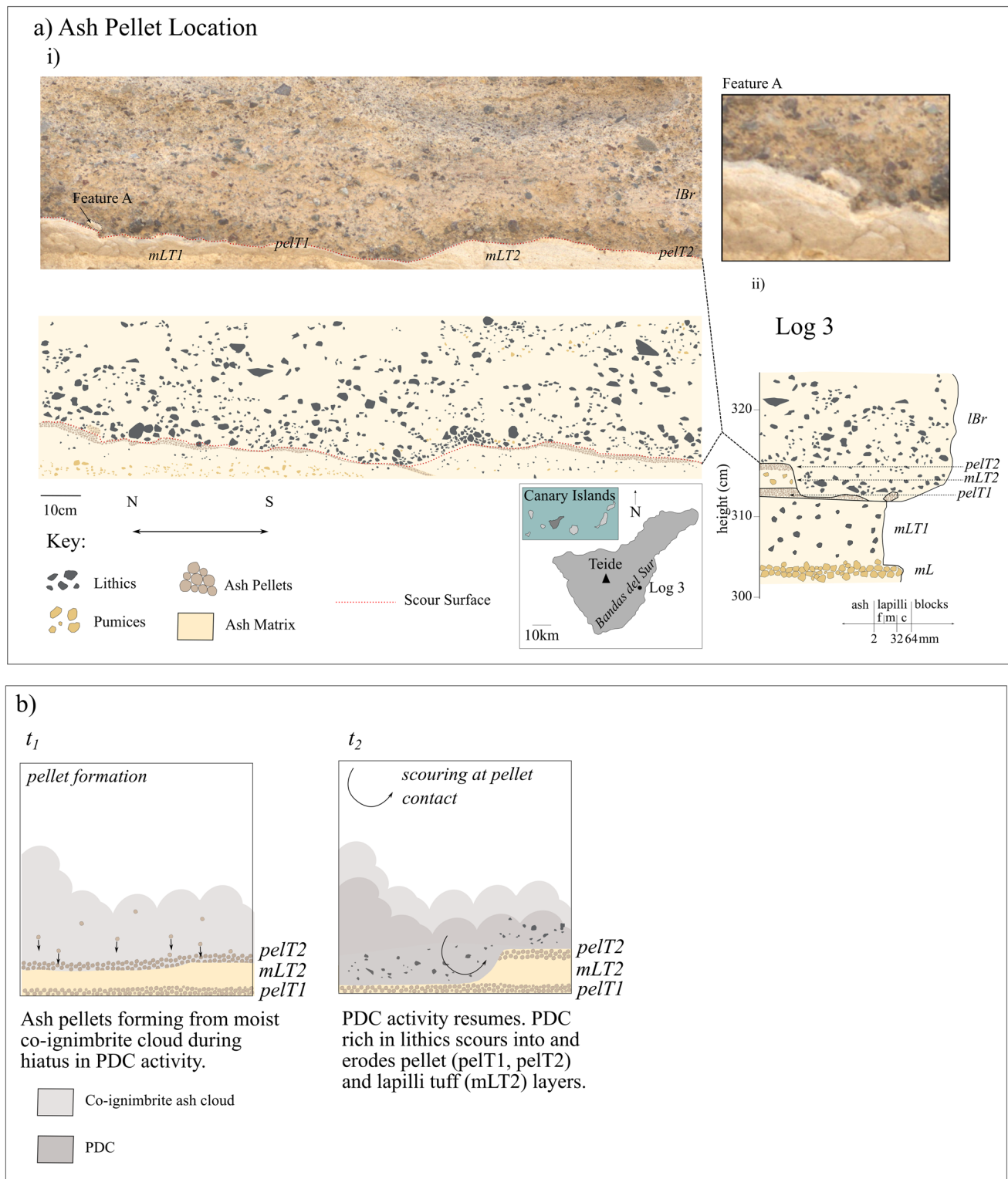


Fig. 5 **a** Ash pellet (pelT1 and 2) layers documenting an episode of PDC hiatus in this area. The ash pellet layers (pelT1 and 2) of the Jurado Member of the Poris ignimbrite (Brown and Branney 2004) are in erosive scouring contact with the lithic breccia (lBr) facies above (red dashed line). **i** Ash pellet contact (pelT1) is overlain by lapilli tuff (mLT2). Feature A indicates remobilisation. The second ash pellet layer (pelT2) is overlain (in erosive contact) by the

breccia unit (lBr). **ii** Location map, log at GR: 2,810,693, 01627006. See lithofacies terminology in Supplementary Material B. Flow direction is north to south. **b** Interpretation panels showing (t_1) the formation of the ash pellet layers and (t_2) erosion of ash pellets and lapilli tuff by subsequent lithic-rich PDC activity (see interpretation text for full explanation)

has previously been attributed to the precipitation of salt or other minerals, which may have caused cementation of the ash (Zeolite, Brown and Branney 2004; Mueller et al. 2017), or from “baking” of the lapilli when moving through high-temperature areas of the PDC during lofting (Brown and Branney. 2004). A lack of fragmentation within the accretionary lapilli layer (mTacc) beneath the contact zone suggests that when the facies was deposited, the current was sufficiently dilute as to not induce breakage (Mueller et al. 2017).

The upper contact between the diffuse stratified accretionary lapilli (dsTacc) and lapilli tuff layer (mLT) contains fragmented accretionary lapilli with some directional fabric to them. This indicates that the current conditions were concentrated and sufficiently energetic to enable interactions and breakage (Mueller et al. 2017). This may be due to tractional processes during the deposition of the fragments, or through cryptic remobilisation by subsequent current activity. In addition to these fragmented lapilli, intact, non-sheared accretionary lapilli are also observed, protruding from the ash layer without signs of erosion from the overriding current (Fig. 4.ii).

“Wet” ash pellet layer contact

At the Poris Quarry, distinct layers of pellets are present that are associated with the Jurado Member of the Poris Formation (Brown and Branney 2004) and a sequence containing ash pellet-rich tuff (pelT) is observed (Fig. 5a). A massive lapilli tuff facies (mLT1), characterised by a poorly sorted lithic and pumice lapilli within an ash matrix, occurs in contact with a pellet-rich ash layer (pelT1). Another lapilli tuff layer (mLT2) occurs above this, in sharp contact with the pellet layer below with little evidence of erosion, and is overlain by a second ash pellet layer (pelT2). All of these units are discontinuously preserved due to erosive contact with an overlying lithic-rich facies (IBr). This lithic breccia facies is observed cutting down into the sequence, with an undulous, scouring contact at its base (indicated by dashed red line in Fig. 5a.i), and in some places both pellet layers are completely absent. In one location (Feature A, Fig. 5a.i), a clump of the first pellet layer is seen to be detached and rotated from its original stratigraphic position within the lithic breccia facies.

Interpretation

The ash pellet layers (pelT1 and pelT2) at Poris Quarry represent direct fallout from a moist co-ignimbrite plume (Fig. 5b) (Brown and Branney 2004, 2013; Brown et al. 2010), marking a hiatus in PDC activity. Unlike accretionary lapilli, ash pellets do not loft within the turbulent PDC, so their deposition signifies a temporary break in PDC activity

in this area. Furthermore, the pellets identified in this area are considered moist on deposition due to the lack of internal laminations and evidence of amalgamation with surrounding pellets (Brown and Branney 2004).

The lapilli tuff layer (mLT1) indicates PDC activity in the area followed by a hiatus ash pellet layer (pelT1). The second lapilli tuff layer (mLT2) indicates resuming PDC activity but is not seen to erode the underlying ash pellet layer (pelT1) (Fig. 5a.i). This facies is overlain by the second ash pellet layer (pelT2) marking further hiatus. Activity then resumes, and a lithic-rich, erosive current scours into, remobilises (Feature A), and sometimes completely removes, the underlying layers (Fig. 5, pelT1, mLT2, and pelT1). It is possible that, prior to the lithic-rich activity recorded here, other facies were deposited and completely removed from the record due to this erosion. However, lithic-rich facies have been linked to waxing current activity (as a result of events such as incremental caldera collapse) elsewhere in the Poris Formation (Brown et al. 2003; Smith and Koke-laar 2013), and it seems sensible to infer that PDC activity resumed at this location following a period of hiatus due to current waxing, marked by increased lithics.

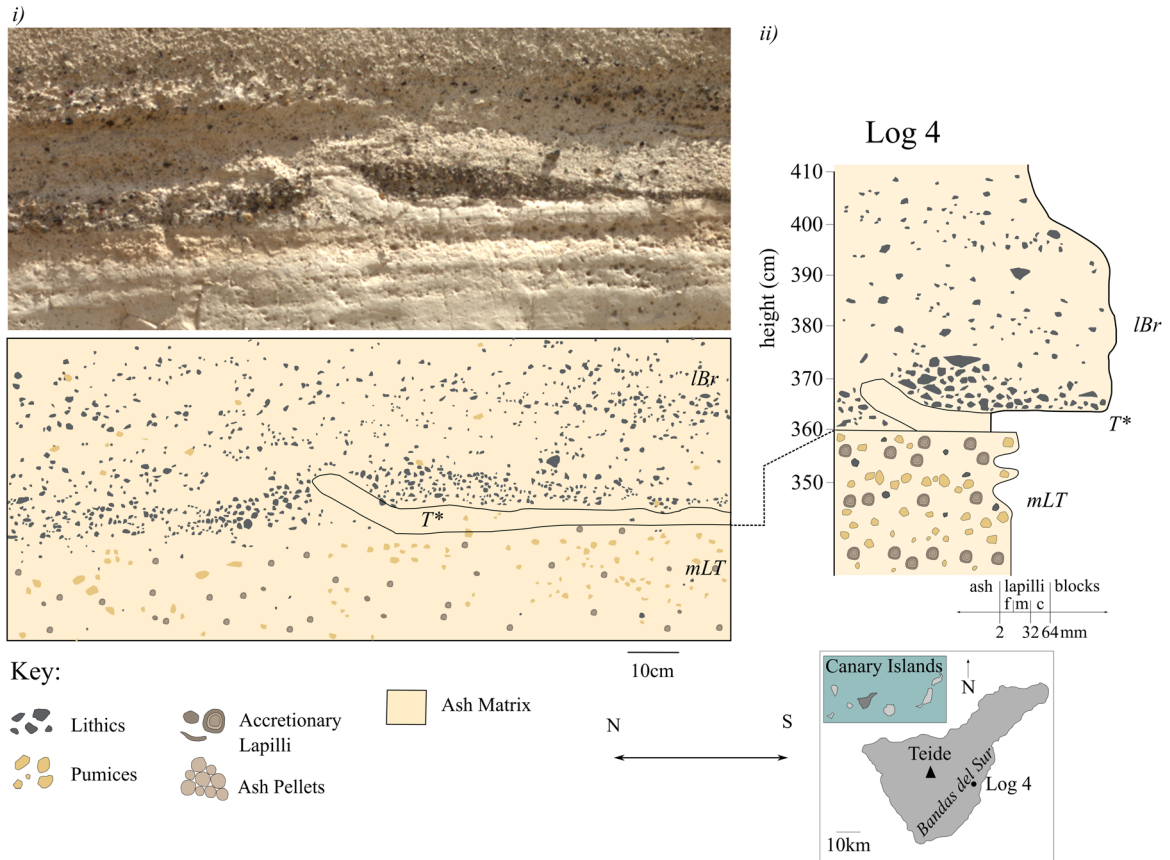
The nature of the relationship between the lithic breccia facies and the ash layers below is a strong indication that these lithics were responsible for the erosion (as opposed to the erosional surface marking an episode of scour and bypass onto which lithics from subsequent activity were deposited). Feature A (Fig. 5a) is particularly important. It shows the remobilisation of a portion of the pellet layer as a “rip-up clast,” indicating a dynamic, shearing depositional environment at the interface between the lithic-rich current and the ash pellet (pelT1) layer. The ash pellet (pelT1) layer must have had an inherent strength to remain intact as a coherent package and to withstand shearing.

Ash layer remobilisation

A buff-coloured and fine-grained ash layer (T*) occurs in the Poris Quarry [GR: 2,810,696, 01627001]. It is observed between a lapilli tuff facies below (mLT) and a lithic breccia facies above (IBr) (the lithic-rich Tamadaya Member of Brown and Branney 2004).

The ash layer (T*) is high in the sequence (~ 5 m above the ground), so the presence of ash aggregates could not be observed. However, a “*” notation is used here to indicate the high likelihood that this facies contains ash pellets or accretionary lapilli, due to its position at a similar stratigraphic level as other pellet layers in the sequence, and from descriptions in Brown and Branney (2004). The ash layer (~ 10 cm thick, and traced for ~ 2.5 m) is distinctive because it exhibits a zone of unique “peeling” and “lifting” in a hockey-stick shape.

a) Ash layer location



b) T* layer remobilisation

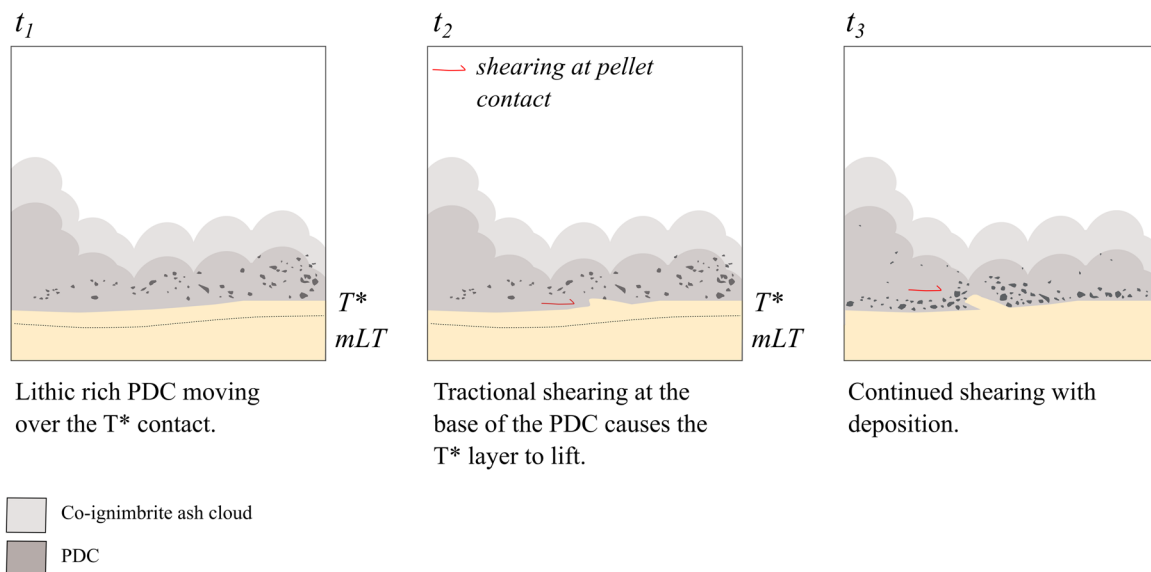


Fig. 6 a.i Ash layer (T*) in contact with overlying lithic-rich facies (lBr) in the Jurado and Tamadaya Member of the Poris Ignimbrite (Brown and Branney 2004) at the Poris Quarry location. Note the ‘peeling up’ and lifting of the coherent zone of ash. **ii** Location map, log at GR: 2,810,696, 01627001. See lithofacies terminology in Supplementary Material B. Flow direction is north to south. **b** Interpretation panels showing the formation of this striking feature at the ash layer contact (see text for full explanation)

Interpretation

The ash layer (T*) is interpreted to record fallout from a moist co-ignimbrite plume during an episode of hiatus in main current activity (Fig. 6b.i; Brown and Branney 2004), similar to the ash pellet layer described in the “Wet” ash pellet layer contact section (Fig. 5). The ‘hockey-stick’ structure (Fig. 6a) is interpreted to record remobilisation of coherent sections of the ash pellet layer due to shearing at the base of a subsequent PDC.

Field observations by Brown and Branney (2004) describe the pellet layers as traceable units, though they are often eroded by subsequent PDCs, leading to inconsistent preservation; this locality provides direct evidence of erosional processes in action. The high lithic content of the breccia (lBr) indicates waxing conditions and the influx of lithics at the source, such as that associated with incremental caldera collapse (Brown et al. 2003; Brown and Branney 2004; Smith and Kokelaar 2013). The interaction of this more concentrated, dense current with the underlying ash layer likely represents a significant change in shear and load behaviours at the flow boundary zone. Despite uncertainty in the nature of the aggregate content, this feature indicates the coherence of this ash layer.

Questions raised by the fieldwork

The field analysis presented here documents ash layers in various contact relationships. One layer, interpreted as ‘dry’ due to a lack of ash aggregates, shows no evidence of resistance to erosion by subsequent activity. Other ash layers, interpreted to have formed under either high or low moisture conditions by their ash aggregate content, are associated with intriguing shear relationships indicating resistance to erosion.

The preservation, or not, of these layers appears to be linked to their inherent strength, which we hypothesise is influenced by moisture content. This raises the question of how moisture influences the strength and, therefore, behaviour and preservation of an ash substrate during subsequent PDC activity. Improved understanding of this issue has implications for our interpretation of volcanic stratigraphy and hiatus layers, particularly for inferences of the number of PDCs formed during an eruption. In the following section, we investigate how moisture affects ash layer strength

and vulnerability to erosion to gain a more comprehensive understanding of the dynamics and preservation of ash layers seen in PDC deposits.

Experimental results

Shear tests were completed to determine how the strength of material changes in dry (0 wt.%) and moist (> 0 wt.%) conditions. We hypothesise that the presence of moisture-induced ash aggregates may increase the yield strength of the material, thereby affecting its ability to be eroded or remobilised.

Direct shear box tests

Direct shear experiments were performed on four samples from 0 to 5 wt.% moisture. The peak stress was not reached during the duration of the experiments (Fig. 7). Therefore, we completed the remaining experiments using the ring shear apparatus, employing finer sized material to better reflect the fine ash as seen in Tenerife. The results of the direct shear box are in Supplementary Material E.

Ring shear tests

The ring shear tests allow us to see the full extent of the shear profile, which was unable to be observed in the direct shear box. The ring shear tests were performed on three samples with 0 and 1 wt.% moisture content.

At 0 wt.% moisture (Fig. 8), Brown Tuff (mean size 3.55 ϕ , 29.35% fines) and Taupo 1 (mean size 2.08 ϕ , 38.90% fines) showed increasing peak shear stress with increasing normal stress (Table 2). The peak shear stress was reached in a 5–20 mm shear distance, although it ran for much longer distances. Atitlan 2 (mean size 3.44 ϕ , 40.57% fines) showed an unexplained decreasing peak stress with increasing normal stress (Table 2, Fig. 8a).

At 1 wt.% moisture, Taupo 1 and Brown Tuff (Fig. 8b, c) again behave as expected, with peak stress increasing with normal stress. Similarly to the 0 wt.% moisture experiments, Atitlan 2 showed an unexplained decreasing peak stress with normal stress (Fig. 8a). The peak shear stress of all 1 wt.% moisture samples was reached in a shear distance of 5–10 mm.

Zones of elastic and plastic deformation separated by a region of yield have been identified (labelled B; Fig. 8). In the elastic zone, material can deform but return, while plastic behaviour occurs when deformation is permanent after exceeding the sample’s yield. Our results show that at 0 wt.% moisture, the region of yielding is consistently reached in the first 16 mm of shearing across all normal stresses. The

Table 1 Experimental material source location, chemical composition, formation mechanisms and the test completed in this work. DS – direct shear, RS – ring shear and DT – drop test. References detail material characteristics, collection and location

Material	Composition	Formation	References	Test
Tung 1, 4, 5, 6 (Tungurahua, Ecuador)	Andesitic	2006 VEI 3 eruption. Sampled at different localities	Hall et al. 2007; Kelfoun et al. 2009; Douillet et al. 2013; Eycheenne et al. 2012	DS – Tung 1,4 and 5 DT – Tung 6
Atitlan 1 (Guatemala)	-	Volcán de San Pedro. Unstudied ignimbrite deposit GR: 14°40'55.24"N, 91°15'29.15"W	Rowley, P. <i>In comms</i> (2023)	DT
Atitlan 2 (Guatemala)	Andesitic	Los Chocoyos eruption (80.6 ka) of Atitlan Caldera. GR: 14°48'54.74"N, 91°12'27.37"W	Rowley, P. <i>In comms</i> (2023)	RS
Brown Tuff (Lipari, Italy)	-	La Fossa Caldera, 80–60 ka. GR: 38°28'46.5"N, 14°57'32.2"E	-	RS
Taupo 1 (New Zealand)	Rhyolitic	253 AD eruption. Sampled 17 km from vent	Wilson (1985)	RS, DT
Taupo 2 (New Zealand)	Rhyolitic	232 AD eruption. Sampled 2–8 km from vent	Wilson (1985)	DT
Colima (Mexico)	Andesitic	Volcán de Colima, México, 2015. GR: 19°43'92.22"N, –103°61'47.05"W	Johnston, T. <i>In comms</i> (2023)	DS, DT
Cornstarch (synthetic material comparison)	Cornstarch	-	Walding et al. <i>in press</i>	DT

average linear displacement required to reach the yield increases with load and decreases with moisture addition.

For the Taupo 1 sample, the application of the Mohr–Coulomb failure shows an internal friction angle of 31° and cohesion value of 0.6 kPa for the dry (0 wt.% moisture) and an internal friction angle of 48° and cohesion value of 1.1 kPa for the 1 wt.% moisture conditions. Brown Tuff results show internal friction angles of 29° and 22° and a cohesion value of 0.56 and 0.42 kPa for 0 and 1 wt.% moisture, respectively. The decrease in values seen for the Brown Tuff may be due to pore-pressure generation. The application of the Mohr–Coulomb failure criterion to Atitlan 2 could not be confidently completed, as increasing normal stresses created negative internal friction and cohesion values. This indicates that another force may be present during the shearing of this material, such as pore-pressure build-up or particle crushing.

Throughout shearing, the results showed a decrease in vertical displacement (compaction) across most samples and moistures. Atitlan 2 is the only sample that shows a dilation (of 0.015 mm), which was recorded at the highest normal stress (20 kPa) at 0 wt.% moisture. However, with increasing shear distance, some granular material was lost through the gap between the two shearing rings (Supplementary Material C), and therefore, the equivalency of shear thinning and compaction was seen.

The ring shear results suggest relationships between the behaviour of the samples under varying moisture levels and normal stresses, highlighting the complexity of their mechanical response. However, Atitlan 2 does not show these relationships.

Particle size and shape analysis

Particle crushing over time may have resulted in fundamental changes in physical particle properties, leading to changes in the shear strength of the sample. To further investigate this effect, particle size and shape (sphericity and symmetry; Table 2), analysis were completed before and after the ring shear experiments (Fig. 8).

Brown Tuff and Taupo 1 showed no apparent change in particle size distribution (PSD) following ring shear experiments, with before and after results. There was also no meaningful change in mean sphericity or symmetry values, which showed a < 0.3% difference compared to the un-sheared sample.

Interestingly, Atitlan 2 shows the most significant change in PSD following ring shear, becoming finer-grained after the experiments (Fig. 9). On the analysis of the shape data, the mean sphericity and symmetry values after 0 and 1 wt.% shearing show a 1% reduction (i.e., more angular and asymmetrical) compared to the un-sheared sample. These results indicate that particle crushing occurred in the Atitlan 2 sample during the experiments. This may have affected the geomechanical properties of the material and may be the cause of the reduced shear strength results for Atitlan 2. This is interesting and could be due to the composition of the material. Previous work by Walding et al. (*in press*) noted that the Atitlan sample in fluidisation experiments showed no significant change in gas escape morphologies with the addition of moisture. This suggests that perhaps the

Table 2 Material properties of both pyroclastic and cornstarch material. These include logarithmic particle size mean and particle size median, particle range, fines content (< 63 µm), and geometric mean (φ). The method of moments is employed for calculating Mean, Sorting, Sphericity, Symmetry, Skewness, and Kurtosis. The Sauter mean diameter is calculated following Beard et al. (2019). Material properties explored further in Walding et al. 2023; in press. The table is ordered by particle size mean

Material	Particle Size Mean (x̄)Ø	Particle Size Median Ø	Particle Size Range (µm)	Fines Content (%)	Sorting Index (σ)Ø	Sorting (σ _G)	Sphericity	Symmetry	Skewness (S/k)Ø	Kurtosis (K/k)Ø	Sauter Mean (mm)	Geometric Mean (µm)
Cornstarch	4.8	4.8	5–340	96.17	0.595	Moderately Well Sorted	0.84	0.91	−0.3	4.3	0.02	35.4
Tung 1	3.8	3.7	2.5–297.3	35.76	0.428	Well	0.77	0.88	1.9	17.0	0.06	72.9
Brown Tuff	3.6	3.4	1–1260	29.35	1.240	Poorly Sorted	0.81	0.88	0.5	3.9	0.05	85.2
Colima	3.5	3.6	10–1000	84.39	1.453	Poorly Sorted	0.72	0.86	−0.5	2.6	0.04	90.3
Atitlan 2	3.5	3.8	< 20–1780	40.57	1.501	Poorly Sorted	0.83	0.91	−0.9	3.2	0.02	92.4
Atitlan 1	2.8	3.1	2–2000	66.03	2.426	Very Poorly Sorted	0.76	0.89	0.1	2.0	0.02	97.2
Tung 4	2.7	2.7	20–650	0.15	0.252	Very well	0.84	0.87	0.1	8.5	0.01	153.5
Taupo 2	2.4	2.3	< 20–2000	52.23	0.979	Moderately Sorted	0.70	0.86	−0.5	4.1	0.04	195.8
Taupo 1	2.1	2.2	< 20–2000	38.90	1.158	Poorly Sorted	0.75	0.87	−0.5	3.3	0.04	234.6
Tung 5	1.6	1.6	10–1000	0.09	0.758	Moderate	0.80	0.87	−0.1	2.5	0.02	347.3
Tung 6	0.8	0.8	10–1000	0.04	0.445	Well	0.79	0.87	0.6	8.3	0.03	557.1

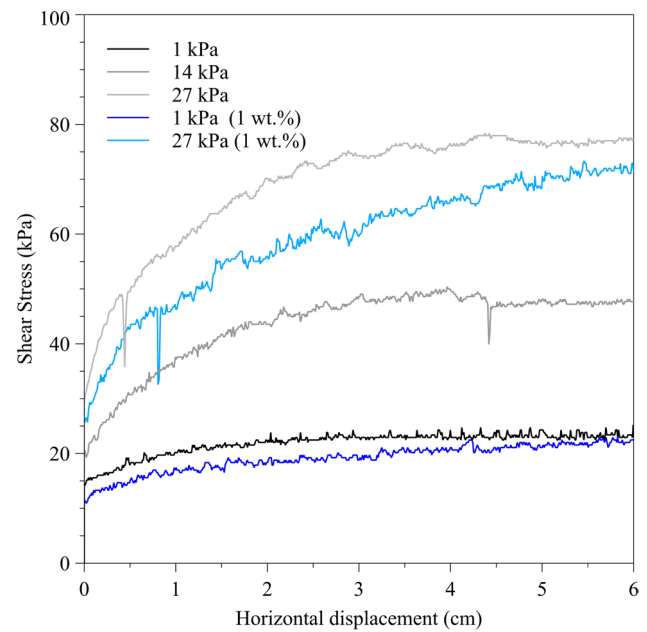


Fig. 7 Direct shear box test of Tung 4 at 0 wt.% (black) and 1 wt.% (blue) moisture contents. Note that the yield stress was not reached. See Supplementary Material E

Atitlan material has H₂O scavenging minerals present or has been hydrothermally altered, ultimately leading to the weakening of the particles, resulting in increased crushing of material. This observation would benefit from future work into the nature of hydrothermally altered ash material and moisture.

Drop tests

Drop tests were carried out to determine whether the rheological properties of ash change at high moisture contents due to the effect known as “shear-thickening” (as seen in cornstarch material). We hypothesise that where ash pellet layers are preserved beneath lithic breccia lithofacies, the impact and shear from the large lithic blocks may induce shear thickening. The increased viscosity may increase the material’s resistance and, therefore, develop a “protection” from the erosion of the dense granular current.

The drop test on cornstarch (96% fine content) at 80 wt.% moisture demonstrated non-Newtonian and shear-thickening behaviour. The steel ball dropped at a speed of 0.16 cm/s, impacting the surface of the mixture and bouncing to a height of 0.55 cm (Supplementary Material F). In the pyroclastic material, two samples showed these same shear thickening behaviours (i.e., bouncing off the substrate deposit) correlated to high fine content.

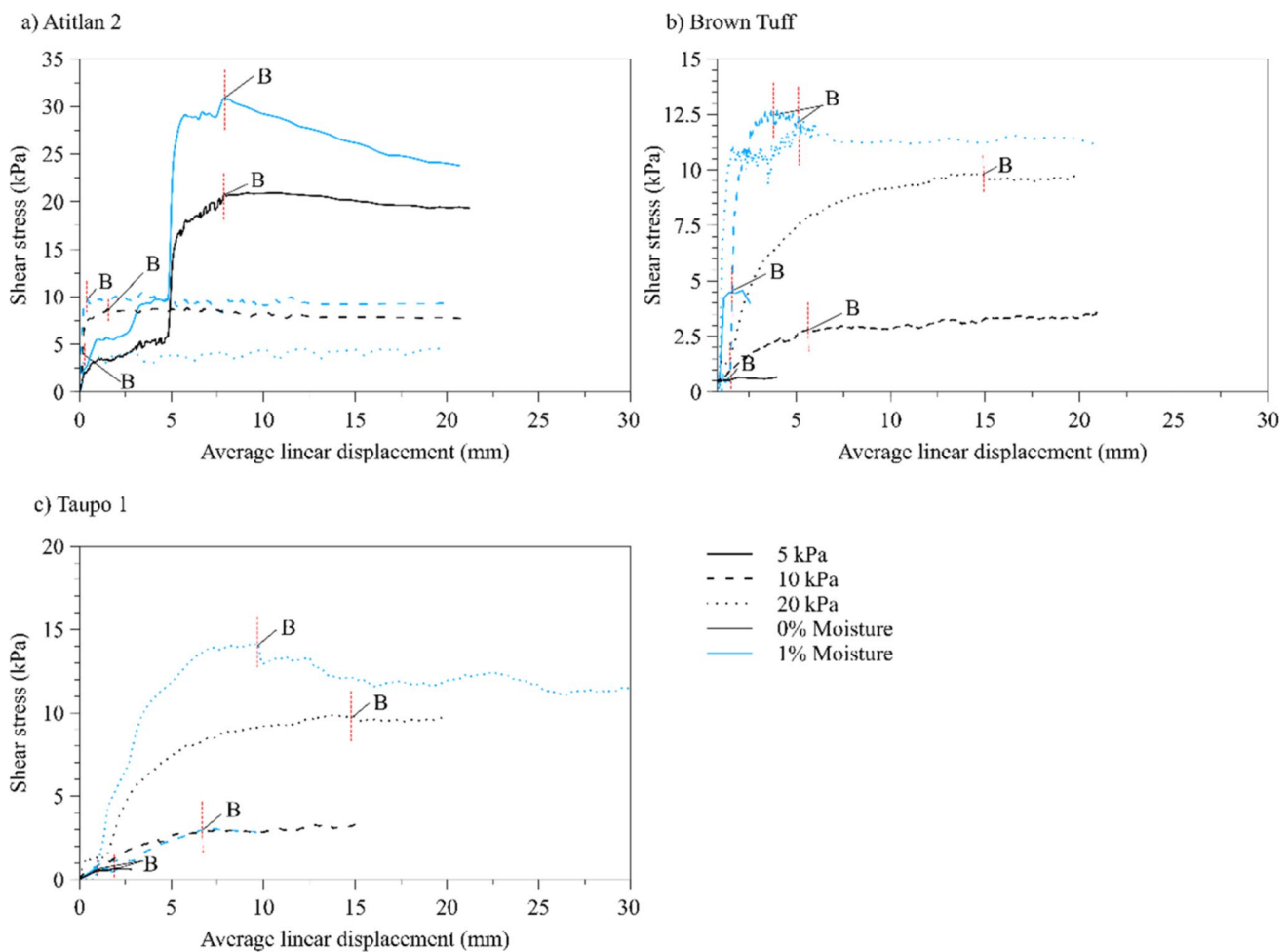


Fig. 8 **a** Atitlan 2, **b** Brown Tuff, and **c** Taupo 1 shearing profiles of material at varying moisture contents (0 and 1 wt.%). (B) shows peak stress, and a dashed red line highlights the yield stress and separates

areas of elastic response (left-hand side of the graph) and plastic hardening (right-hand side of the graph)

The results for pyroclastic materials show that with sufficiently high wt.% moisture, Atitlan 1 (~ 40 wt.%, 66.03% fine content), Colima (~ 25 wt.%, 84.39% fine content), Taupo 1 (~ 50 wt.%, 38.9% fine content), and Taupo 2 (~ 70 wt.%, 52.23% fine content) all show evidence of shear thickening (i.e., a reducing ball penetration depth with increasing moisture and in some cases show the ball bouncing off the surface; Fig. 10, Supplementary Material F). At 50 wt.%, the ball bounced and reached a height of 0.6 cm for the Taupo 1 sample and ~0.6 cm for the 70 wt.% Taupo 2 sample (Supplementary Material F).

When moisture levels were increased above these percentages for each sample, the ball completely penetrated the saturated deposit with little resistance (Fig. 10d).

Shear thickening behaviours were associated only with some finer materials at a limited moisture range. Tung 6 (particle size mean 0.833 ϕ , 0.04% fine content) did not show shear thickening in any experiment; at all moistures

tested (30–40 wt.%), the ball moved straight through the material (Supplementary Material F).

These results demonstrate the ability of pyroclastic material to exhibit changes in strength at varying moisture ranges, dependent upon particle characteristics. The ball moves directly through all samples' deposits at dry or low moisture contents under loose conditions (e.g., Fig. 10b). At high moisture levels (Atitlan 1, > 50 wt.%; Colima, 30 wt.%; Taupo 1, > 60 wt.%; Taupo 2, > 80 wt.%), the material becomes a particle suspension, where the granular material is dominated by particle–fluid interactions (Sosio and Crosta 2009) and the ball moves straight through the deposit (Fig. 10d). Some pyroclastic materials, as seen in Taupo 1 and 2, can show shear-thickening behaviour (Fig. 10c). This is not the case for Tung 6, probably due to its lack of fines content. When impacted or sheared, a shear-thickening material stiffens, which can result in resistance to deformation or penetration (as indicated in our results).

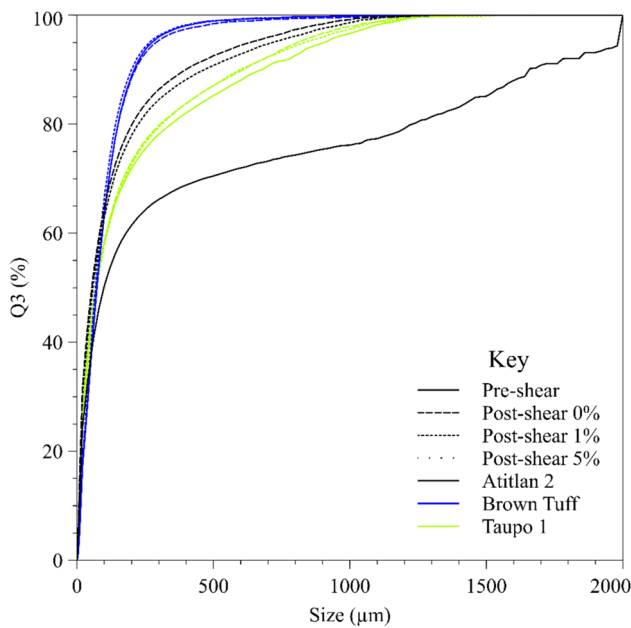


Fig. 9 Particle size analysis of material before and after the ring shear experiments

Discussion

Dry deposit

The dry deposit environment is a baseline comparison since it represents a deposit not influenced by moisture (i.e., lacking accretionary lapilli or ash pellets). A dry ash substrate can form from ash fallout originating from an eruption plume, the fallout of a dry co-ignimbrite cloud or the deposition of a dilute PDC (e.g., Fig. 3a, 11). In such cases, the shear strength and cohesivity of the deposit are low. Variations in shear strength will be primarily influenced by particle packing, particle density and fine content (Roberts et al. 1998; Kimiaghali et al. 2016). Shear strength and

cohesivity will be affected by fines content and grain size, resulting in the formation of Van der Waals or electrostatic forces between particles.

In the field, ash layers that were interpreted to be dry did not show sharp, upper contacts with overriding PDC deposits, nor did they display peeling features or any other features indicative of cohesivity or shear strength. The loose nature of recently deposited ash layers makes them vulnerable to erosion by subsequent PDC activity. As a result, even when thin ash layers are deposited that could record a hiatus and delineate a flow unit (i.e., co-ignimbrite or plume fallout), their low preservation potential makes them unlikely to be recorded in volcanic stratigraphy—resulting in cryptic or missed layers (Fig. 11). Additionally, the erosion of the dry substrate may lead to entrainment and bulking of the overriding current, potentially increasing run-out distances and increasing the hazard risk (Bernard et al. 2014).

Moisture-affected deposits

A moisture-affected deposit is characterised by the influence of moisture, as inferred by the presence of accretionary lapilli and ash pellets. Ash pellets can form from a moist co-ignimbrite cloud or when raindrops interact with ash particles (Fig. 11, Brown et al. 2012; Diaz-Vecino et al. 2022). Consequently, resulting deposits may exhibit a range of moisture contents, from low to potentially saturated levels, either due to the presence of a high concentration of ash pellets or from direct rainfall on the aggrading deposits. Accretionary lapilli is formed by the lofting and cycling of ash pellets between hotter, lower areas, and moister, cooler upper areas of a PDC, which leads to the accretion of thin concentric ash layers (Reimer 1983; Schumacher and Schmincke 1995; Brown et al. 2012; Diaz-Vecino et al. 2023). The final deposits are interpreted as being indicative of general low-moisture conditions. Given that PDCs are typically hot, it is unlikely that these deposits would be uniformly moist or

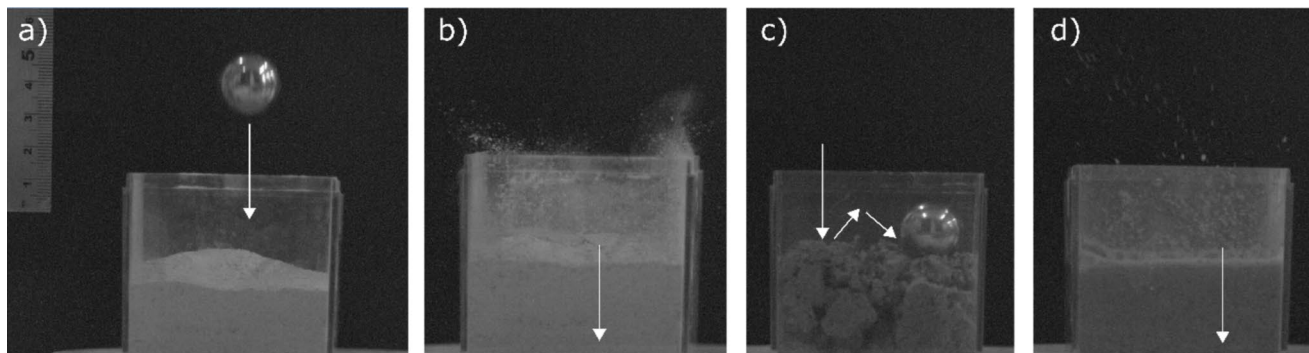


Fig. 10 Drop test completed on Taupo 1 sample at **b** 0 wt.% moisture, **c** 50 wt.% moisture, and **d** 60 wt.%. Arrows show the movement of the ball from **a** falling, **b** and **d** moving through the material and **c** showing the bouncing movement of the ball on impact with the deposit

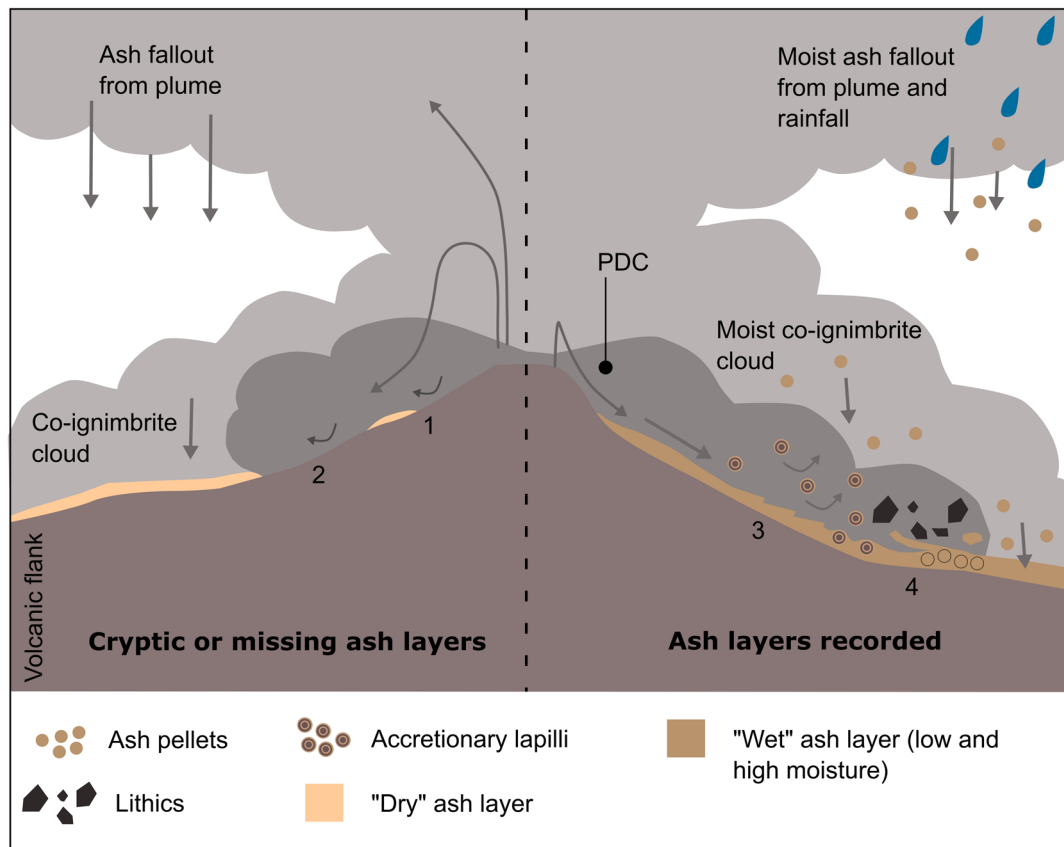


Fig. 11 Schematic showing dry (left) and wet (right) ash layers forming from dry and moist plume fallout, co-ignimbrite fallout and dilute PDC deposition. At the dry locality, a subsequent PDC entrains (1) the loose ash material, possibly leading to bulking (2) in the current. The final deposit shows a cryptic or missing ash layer. In the wet scenario, moisture in the substrate is inferred by the presence of ac-

cretionary lapilli and ash pellets, which lead to an overall more cohesive deposit of greater shear strength (3). Furthermore, where lithics are present (4), high moisture substrates can experience shear thickening. This results in the preservation of “wet” ash layers, which are recorded

saturated, leading instead to spatial variations in moisture content. Furthermore, the presence of water can facilitate salt and mineral precipitation at the particle boundaries, accretionary lapilli can be strong, and energy exerted on them (i.e., from the collision with other particles) can result in their fragmentation or complete disaggregation (Mueller et al. 2017).

In the field, ash layers rich in accretionary lapilli sometimes displayed stepped erosive contacts, where the contact sheared through them, or more diffuse contacts, where the contact wrapped around protruding accretionary lapilli. For the accretionary lapilli to be sheared through, they and the surrounding unconsolidated ash must possess sufficient inherent strength to resist disaggregation and erosion despite having only recently formed. Additionally, the presence of protruding accretionary lapilli that were not plucked out by the overriding current, suggests that the lapilli are strong (Fig. 11). Laboratory experiments with low moisture conditions support these field observations, where moisture increase from 0 to 1 wt.% in pyroclastic

material increases the yield strength and, therefore, resistance to shear (Fig. 11).

In contrast, ash pellet layers often formed sharp contacts with overlying lithic-rich deposits and, in some cases, were seen to be ‘lifted’, ‘peeled up’ or incorporated as clasts, indicating a greater shear strength within the deposit, allowing for coherent remobilisation of these layers. These features are reminiscent of deformed laminations and rip-up clasts of mud layers seen within turbidite sequences. Such features occur in turbidite sequences when cohesive sediments, like clay, bind together and are subsequently eroded and transported (Allen 1982; Li et al. 2017; Yang et al. 2024).

The erosion of mud-rich sediments requires a critical shear stress to initiate substrate erosion (Chen et al. 2021a, b). Particle size plays a crucial role in influencing a material’s erosional potential; for example, clay-rich materials exhibit greater cohesion compared to sand-dominated, granular materials. In addition, experimental studies have demonstrated that cohesive sediments erode as aggregates under low bed shear stresses or as ‘clasts’ of material under

higher shear stresses (Sanford and Maa 2001; Le Hir et al. 2011; Chen et al. 2018; 2021a, b, and references therein).

The results from the shear experiments (Fig. 8b, c) show that increasing moisture (1 wt.%) led to an increase in the yield strength. The elastic limit is reached in less time than the dry material in the 1 wt.% substrates (Brown Tuff and Taupo 1). This indicates that the 1% material is deforming over shorter periods of time, but with more yield strength required to do so than material at lower moisture content. The separation between plastic and elastic deformation may also explain the remobilisation structures seen. For example, the elastic deformation (i.e., connected to the base and being “peeled” up) of the feature in Fig. 7 and the more plastic deformation (i.e., the brittle separation from the underlying substrate) of feature A in Fig. 6. Furthermore, at high moisture contents (25–70 wt.%), the drop tests revealed that a ball will impact and bounce off a deposit, resulting in less penetration. This reveals compelling evidence of shear thickening in a high-moisture pyroclastic material, leading to the dynamic preservation of high-moisture layers in high-stress environments. This behaviour, commonly seen in dense suspensions of solid particles, illustrates the complex rheological response of ash deposits, which can transition from easy flow at low shear rates (as determined by the shear experiments) to solid-like resistance at higher shear stresses (drop tests). In volcanic successions, this process may explain the resistance of thin ash pellet layers to erosion by more significant, caldera-forming deposits, such as lithic breccia.

Implications for interpreting PDC stratigraphy and hazard

This work demonstrates the influence of moisture on the preservation of ash layers that can be important marker horizons (Fig. 1) and finds that ash layers formed in low or high moisture conditions are more likely to be preserved than those formed in dry conditions (Fig. 11).

These findings have important implications for interpreting ash layers in volcanoclastic sequences, which can record episodes of PDC hiatus and delineate flow units. A lack of understanding of the preservation potential of an ash layer could lead to an overestimation or underestimation of the number of flow units in a deposit, relevant to interpretations of the location of PDC hazard through time. Furthermore, understanding the likelihood of erosion and incorporation of a fine-grained ash substrate into a PDC is non-trivial; the entrainment of dry, loose material can promote flow bulking of PDCs, resulting in increased flow mobility, higher velocities and extended runout distances (Iverson 2012; Bernard et al. 2014).

Future research should focus on understanding deposit variability in order to determine how natural changes in the

substrate affect entrainment, thereby contributing to current bulking and the removal of key deposit layers. Additionally, further investigation into the rheological behaviour of pyroclastic materials under varying moisture and shear conditions would provide a more precise understanding of shear thickening behaviour. This is important in understanding the erosion processes that might lead to flow-bulking and associated modifications to flow hazard. Finally, when reassessing past deposits and conducting future studies, it will be crucial to consider the role of cohesion in layer preservation and incorporate this factor into stratigraphic field interpretations.

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Declarations

Competing interests The authors declare no competing interests.

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